



**United Technologies
Research Center**



Water Mist-Based Fire Suppression Modelling of an Office Space Scenario

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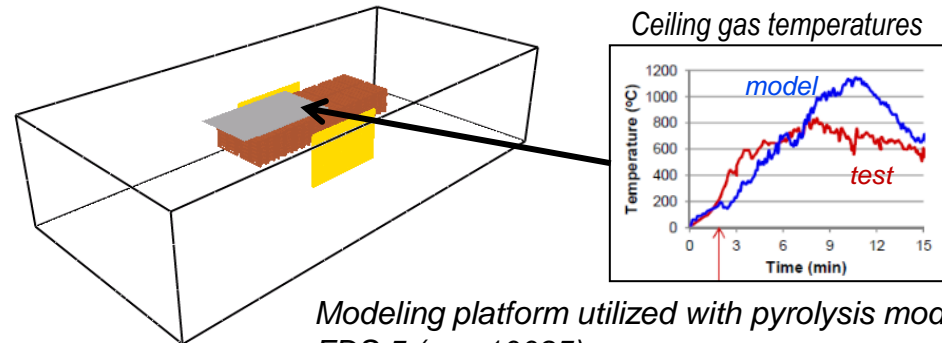
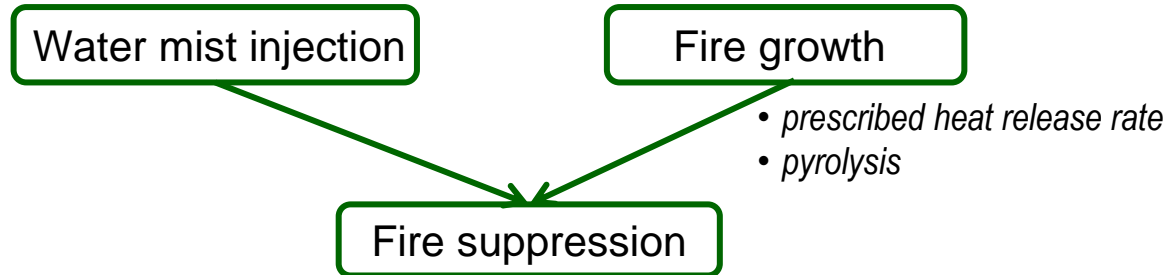
**14th International Water Mist Conference, Istanbul, Turkey
October 22-23, 2014**

BACKGROUND

Motivation: Develop modeling methodology that provides physical understanding into water mist fire suppression → enable efficient test planning and execution

Previous large scale simulations: Ro-Ro Deck Fire with Cooling Mist

Simulation approach



Reference: SupDet 2013, "Modeling water-mist based suppression of 34 GJ car-deck fires using FDS"

Can we apply the same methodology to simulate other fire test scenarios?

OBJECTIVE

Demonstrate a modeling approach that simulates a water mist-based fire suppression of the European Ordinary Hazard I office space scenario.



Fire load includes:

Wood

Paper

Plastics

Foam

Water mist injection:

*Marioff HI-FOG[®] 2000
sprinkler*

OVERALL MODELING APPROACH

Water mist injection



- Droplet injection
- Air entrainment
- Droplet transport

Fire growth



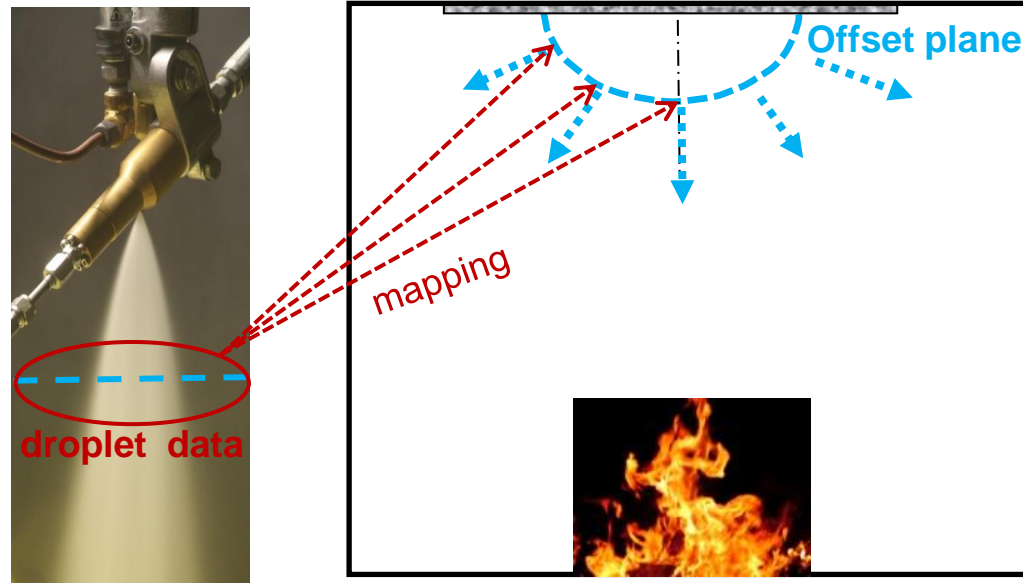
Water mist-based fire suppression



*Modeling platform utilized in office space simulation:
FDS 6 (svn 17743)*

WATER MIST SPRAY INJECTION

Approach



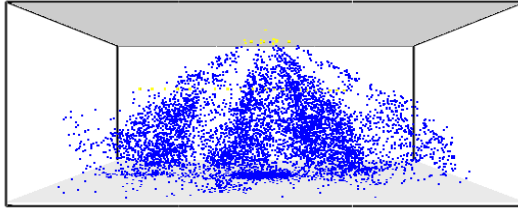
- 1) Measure experimental data from single spray jet near the exit
- 2) Scale measured droplet number densities and velocities to conserve mass and momentum
- 3) Inject spray distribution with prescribed drop size and velocities at the offset plane
- 4) Use gas velocities from spray data to represent entrained gas motion

Reference: SupDet 2011 presentation, "A novel approach for simulating droplet transport for watermist applications"

WATER MIST SPRAY INJECTION

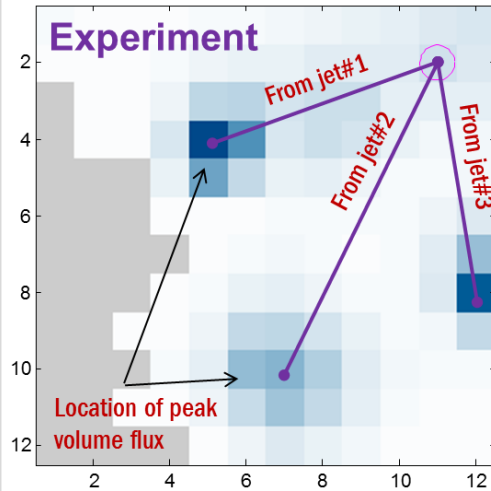
Cold spray simulation of the HI-FOG 2000 sprinkler verified with spray data

Droplet dispersion from Marioff HI-FOG 2000 sprinkler

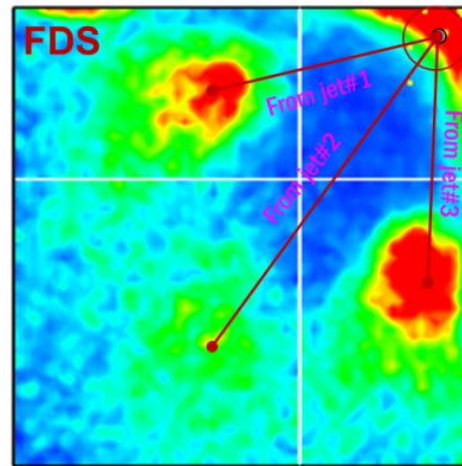


Mesh number	Mesh resolution (cm)	# cores	Simulated test period (sec)	Wall clock time (hrs.)
720,000	5	9	10	1.4

Water flux distribution

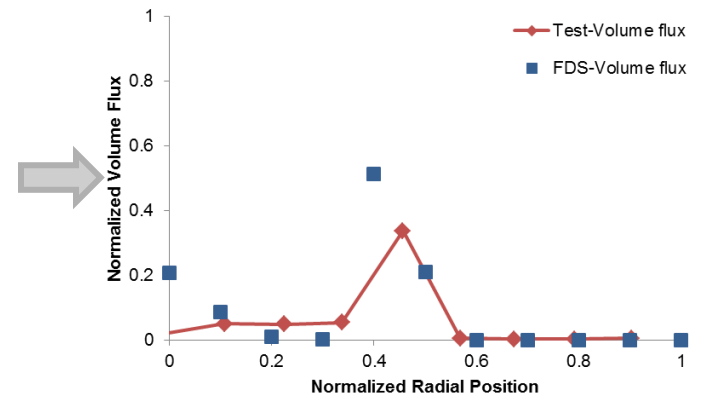


Patternation measurement (top view)



Accumulated Mass Per Unit Area (AMPUA) from simulation (top view)

Volume flux profile through jet#1



OVERALL MODELING APPROACH

Water mist injection



Water mist-based fire suppression



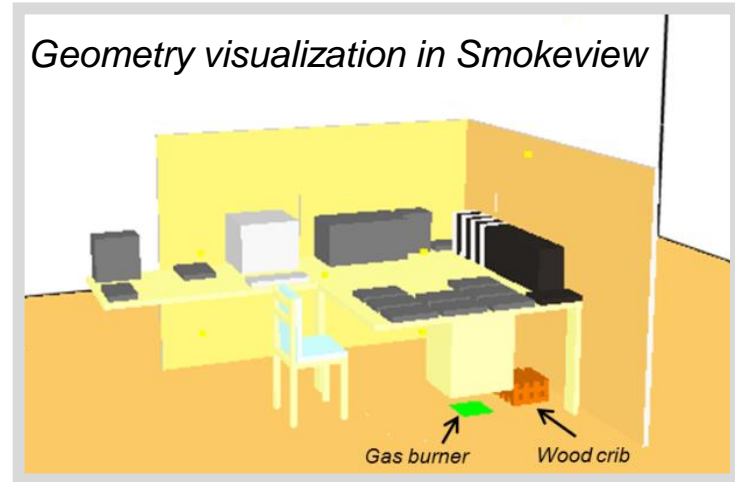
Fire growth



- Fire ignition
- Fire growth

OFFICE SPACE: FIRE GROWTH

Realistic fuel package set up in a large domain with a non-uniform grid

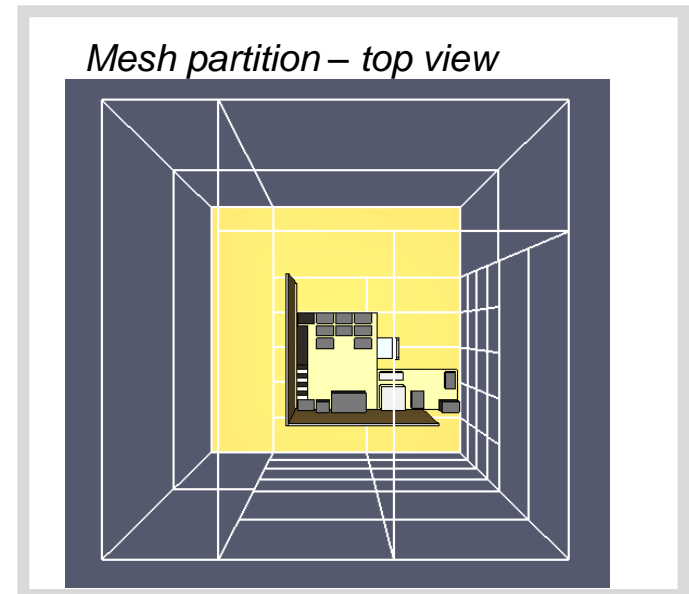


Computational domain (L x W x H): 5.12 m x 5.04 m x 4.96 m

Non-uniform grid:

- 4 cm hexahedral mesh surrounding fuel package
- 8 cm mesh away from the table

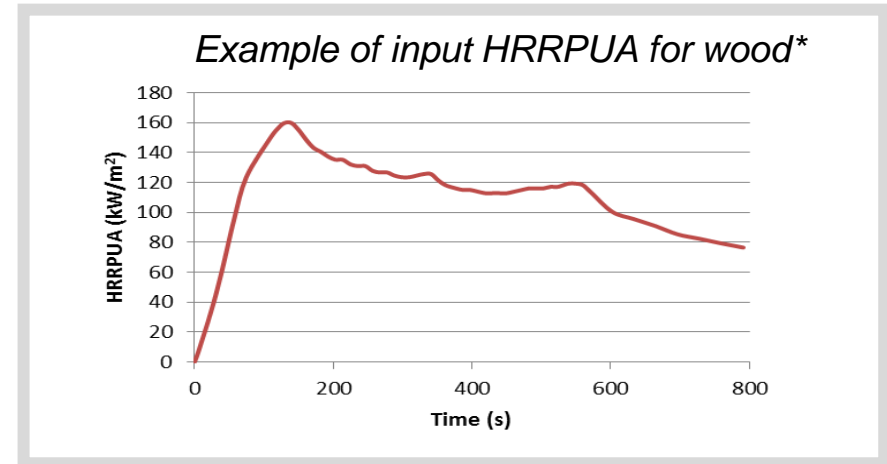
Parallel simulation on 48 computing processors



OFFICE SPACE: FIRE GROWTH

Approach: prescribe a heat release curve and ignition temperature for each material

Tune HRRPUA magnitude and ignition temperature for each material until fire growth is matched qualitatively.



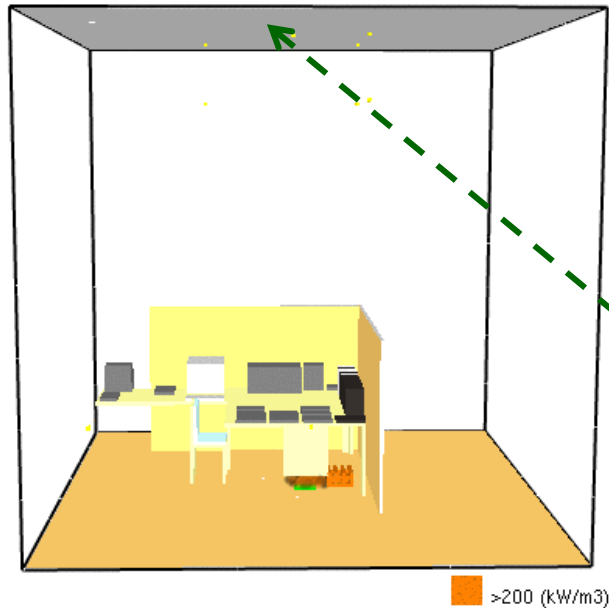
*Based on scaled U.MD wood crib test data
Reference: "Suppression Effectiveness of Water Sprays on Accelerated Wood Crib Fires", Bryson Jacobs, University of Maryland, 2011

Case	Mesh number	# Cores	Simulated test period (Sec)	Wall clock time (Hrs.)
Fire growth simulation	734,000	48	800	32

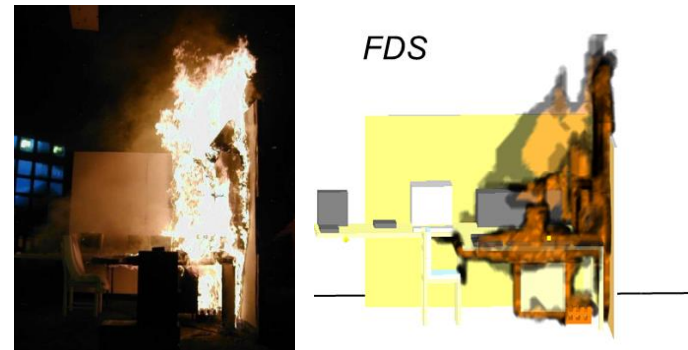
OFFICE SPACE: FIRE GROWTH

Simulation verified with fire size image, ceiling gas temperatures from free burn case

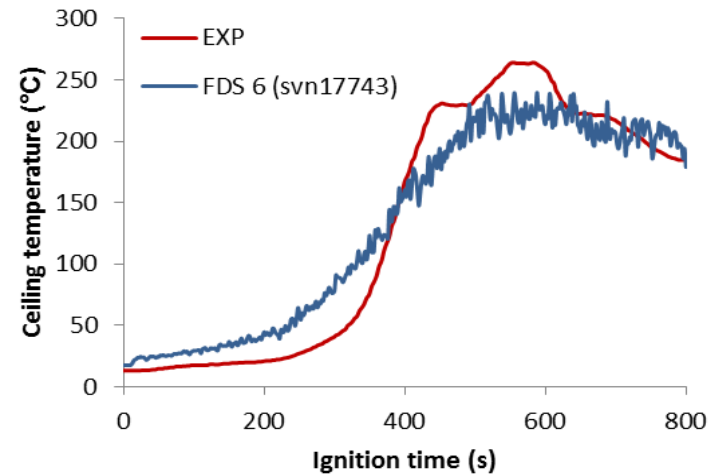
Fire growth—free burn



Verification: fire size at 435s after ignition



Evolution of ceiling gas temperature



OVERALL MODELING APPROACH

Water mist injection



Fire growth



Water mist-based fire suppression



Primary suppression mechanisms

- Gas phase extinction
- Reduction of burning rate via wetting

OFFICE SPACE: FIRE SUPPRESSION

Set-Up: Under 1 sprinkler simulation

For each material, prescribe

- Heat release rate per unit area (HRRPUA)
- Ignition temperature

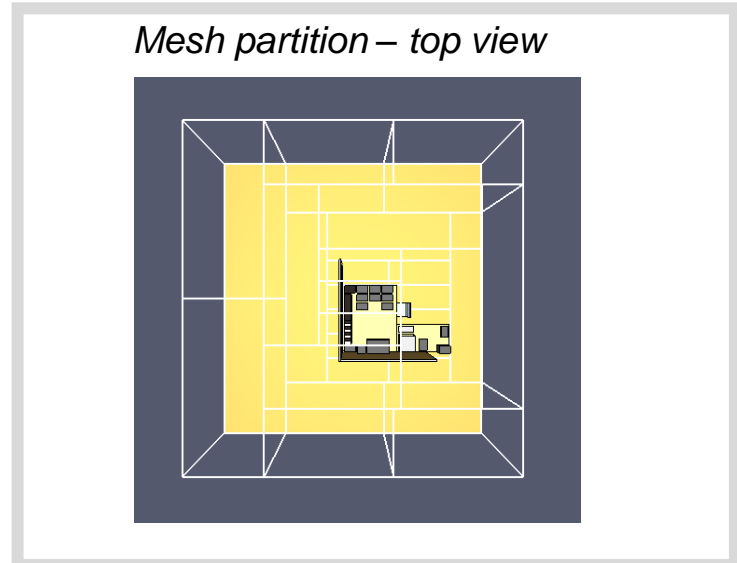
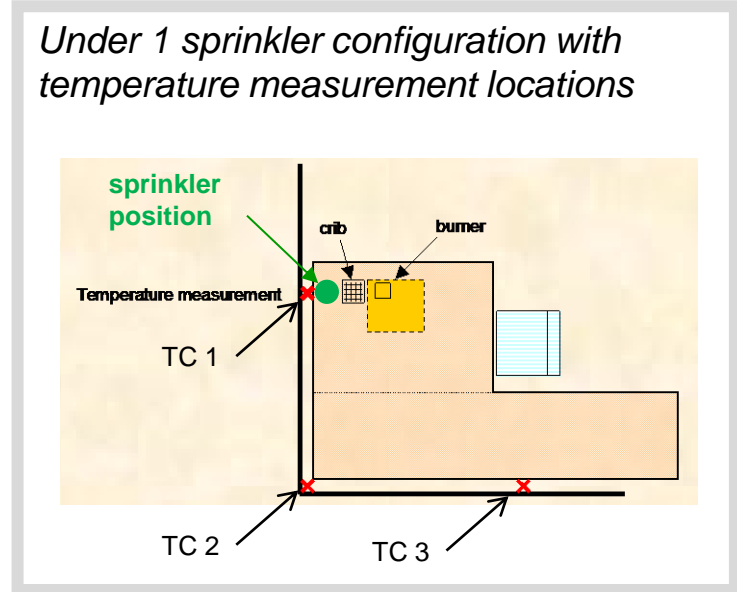
Computational domain (L x W x H): 8 m x 8 m x 3.52 m

Non-uniform grid:

- 4 cm hexahedron mesh surrounding fuel package
- 8 cm mesh away from the table

Parallel simulation on 36 computing processors

sprinkler activation: set at 159s after ignition



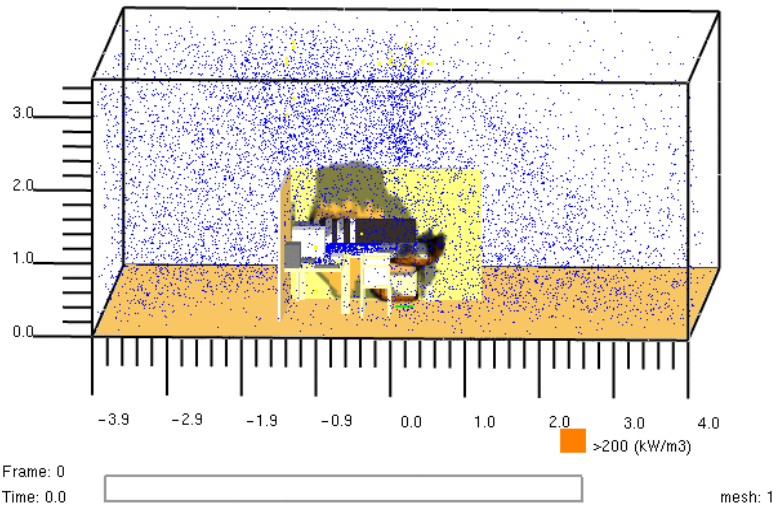
Case	Mesh number	# Cores	Simulated test period (sec)	Wall clock time (hrs.)
Fire suppression simulation	978,000	36	800	160

OFFICE SPACE: FIRE SUPPRESSION

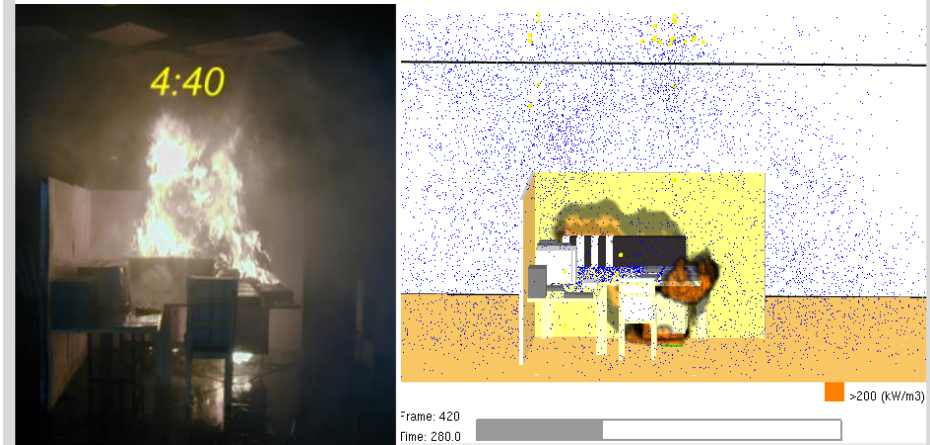
Under 1 sprinkler suppression case demonstrated; suppressed fire size trend captured

Modeled fire growth and spray suppression

Smokeyview 6.1.5 - Dec 26 2013



Flame shape at 280s after ignition

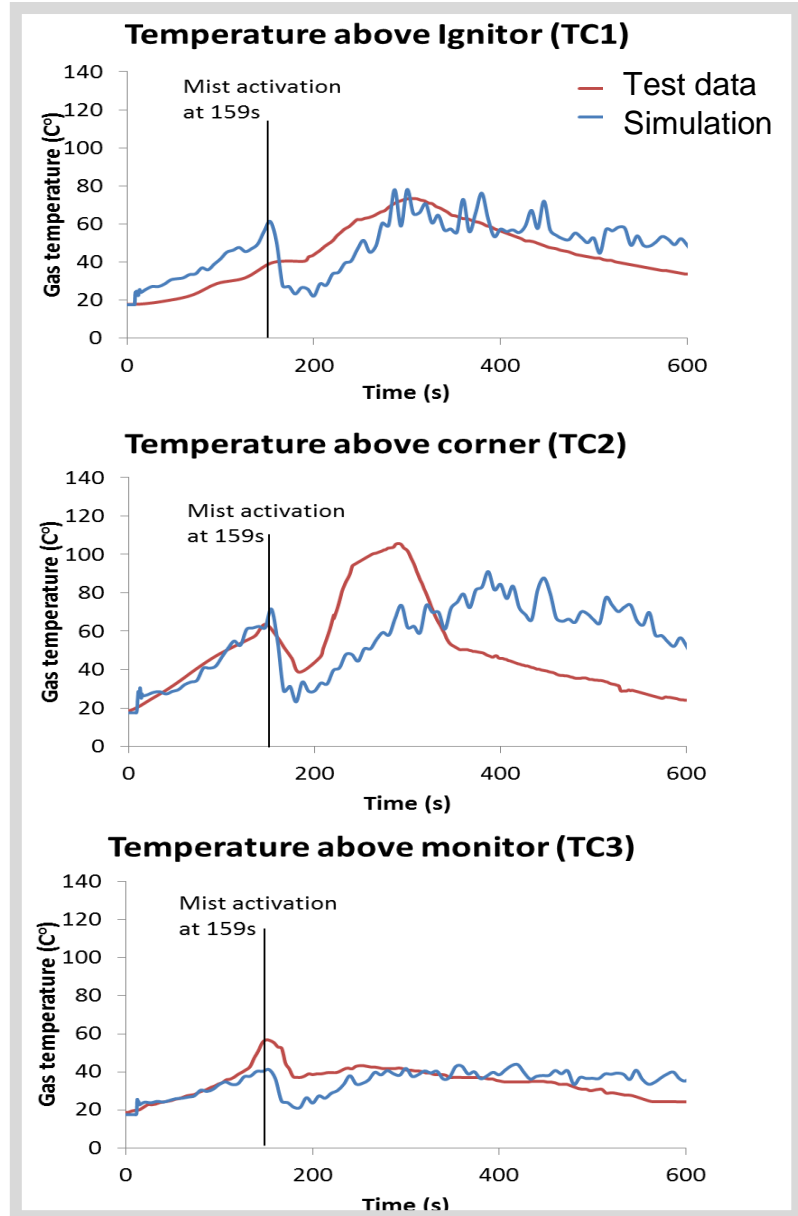
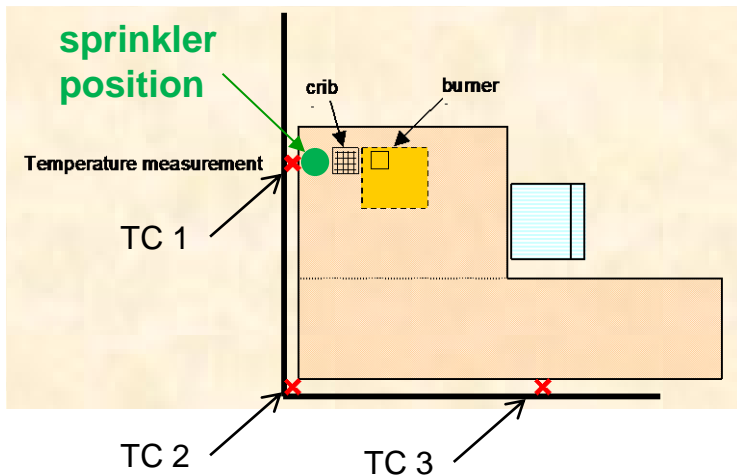


Test image

FDS result

OFFICE SPACE: FIRE SUPPRESSION

Ceiling gas temperature trends captured by simulations



Summary

- A simulation of the European Ordinary Hazard Group 1 Office Space was successfully demonstrated and verified with limited fire test data
- Modeling methodology used FDS 6 as a platform and included the following:
 - ❑ Defining the spray with experimentally-derived measurements of drop size, velocity, and entrained gas
 - ❑ Defining the fire growth of different fuel load types (wood, paper, plastics, foam) with unique heat release rates and ignition temperatures
 - ❑ Applying the extinction model and wetting

Thank you!

Questions?

Modeling & Numerical Considerations

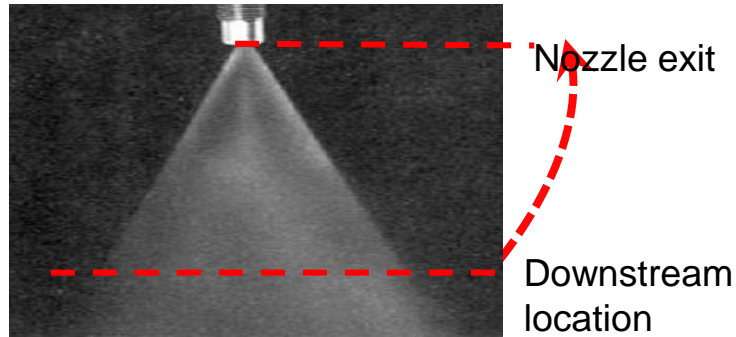
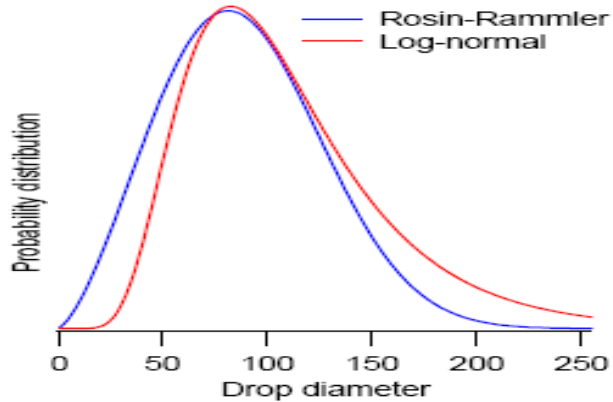
Fire Dynamics Simulator (NIST)

- Eulerian-Lagrangian approach for multi-phase physics
- Dynamic (or constant) Smagorinsky large eddy solver
- Finite rate reaction, a mixing controlled reaction, or a mixed-mode reaction
- Low Mach number assumption
- Low oxygen-limit flame extinction model
- Radiation solver – gray gas, wide band model, Mie theory for scattering/absorption

Water – Mist modeling

Traditional approaches:

- Apply downstream droplet distribution at **nozzle exit**



- Set droplet velocity based on flow-rate
- “Iterate” to match downstream profile

Disadvantages:

- Require non-trivial tuning for different nozzles & conditions
- Near nozzle simulation expensive and poses substantial numerical challenges
- Can violate conservation laws