

Breaking the
“Standard” cycle:
The case for
electronic activation

21st IWMA Conference Madrid



Agenda



Yusuf Muhammad
Chief Design Officer

1. Mechanical activation and the fire industry
2. Why we need innovation?
3. The automotive and aerospace industry
4. The fire engineering case for electronic activation



Mechanical activation



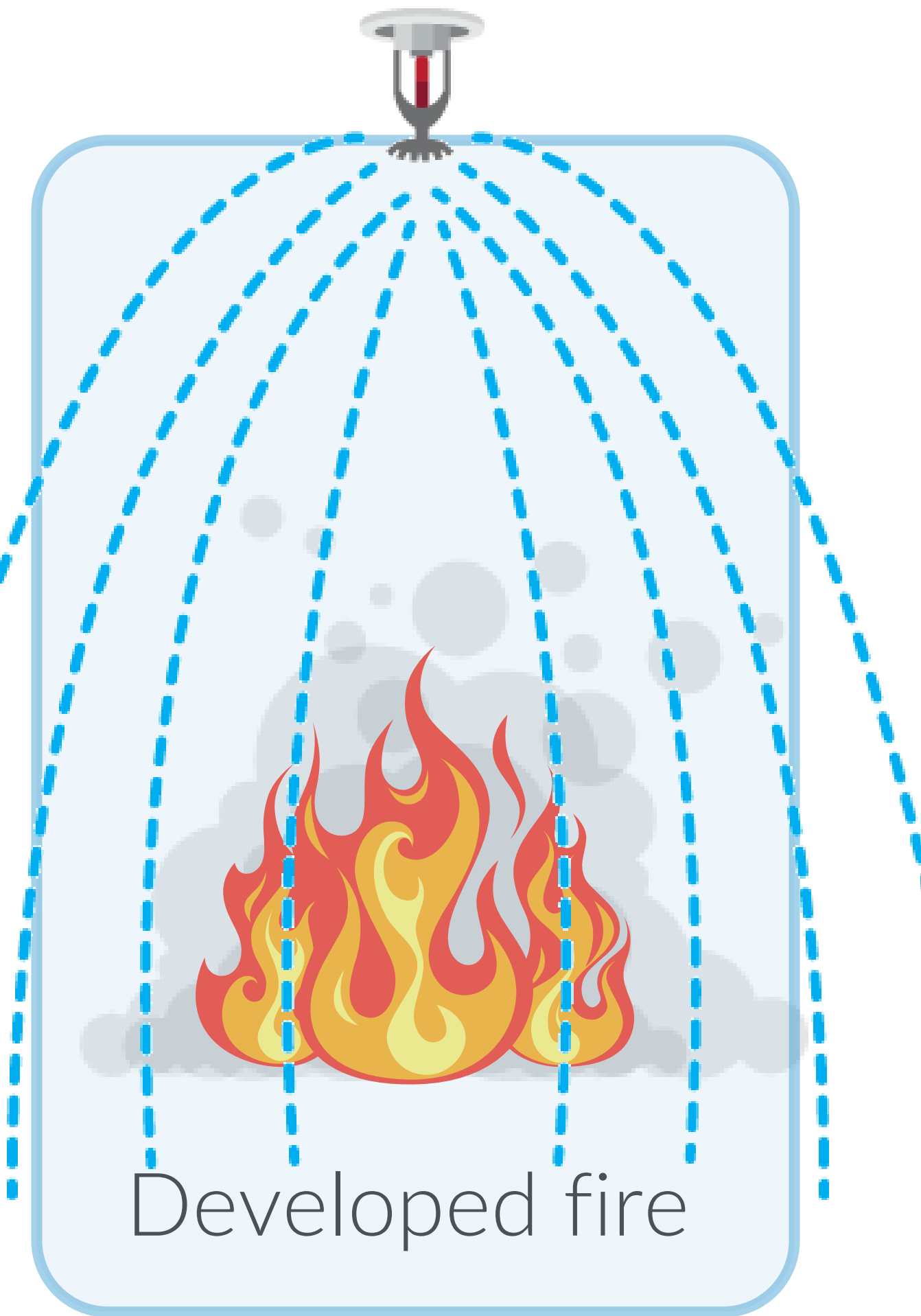
Pre incident



Incipient stage



Growing fire



Developed fire

Objective of Active Fire Suppression

Adequate level of occupant safety

Limiting physical damage to the building

Facilitation of firefighting

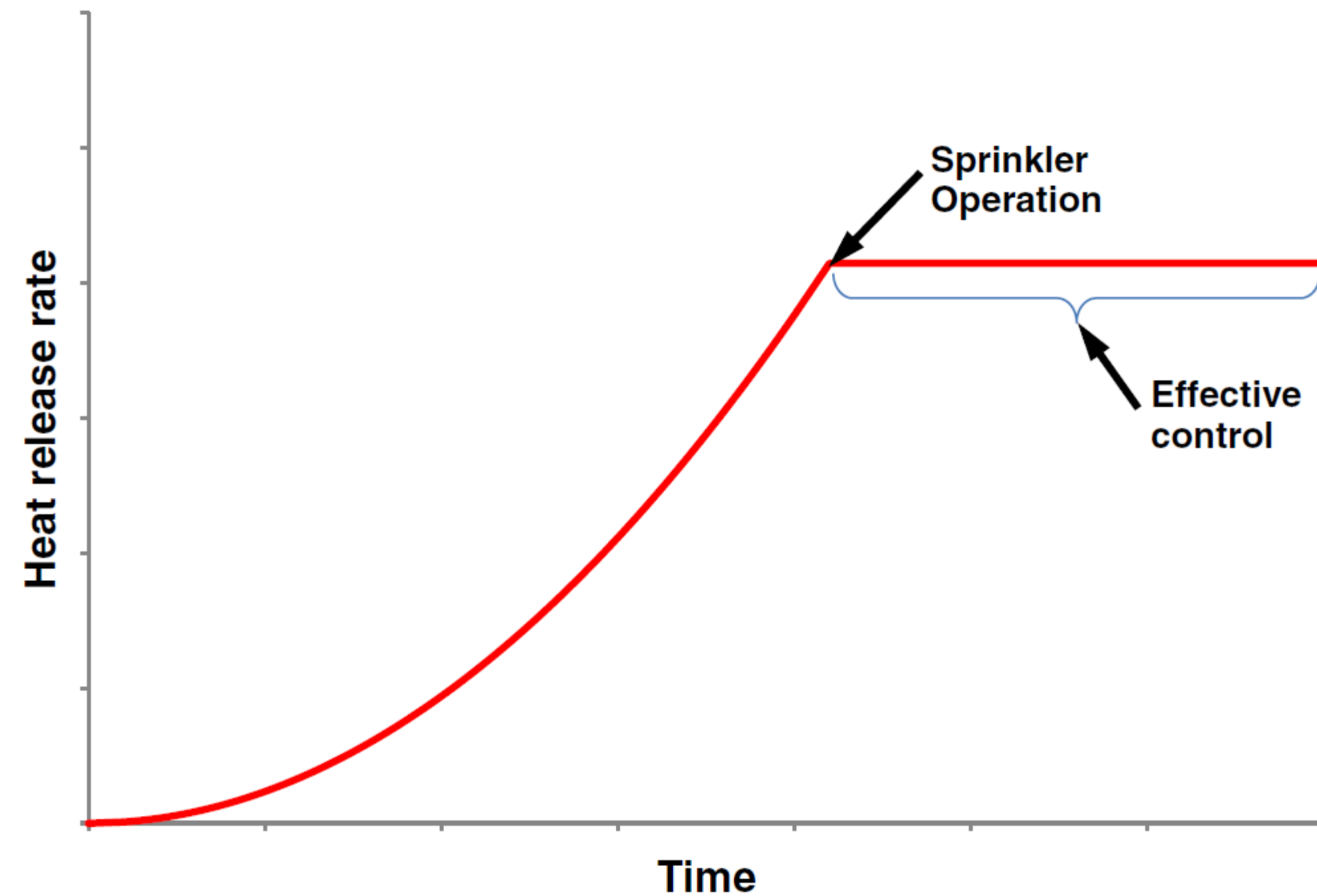


Figure 2 A commonly assumed heat release rate curve for sprinkler fire control.

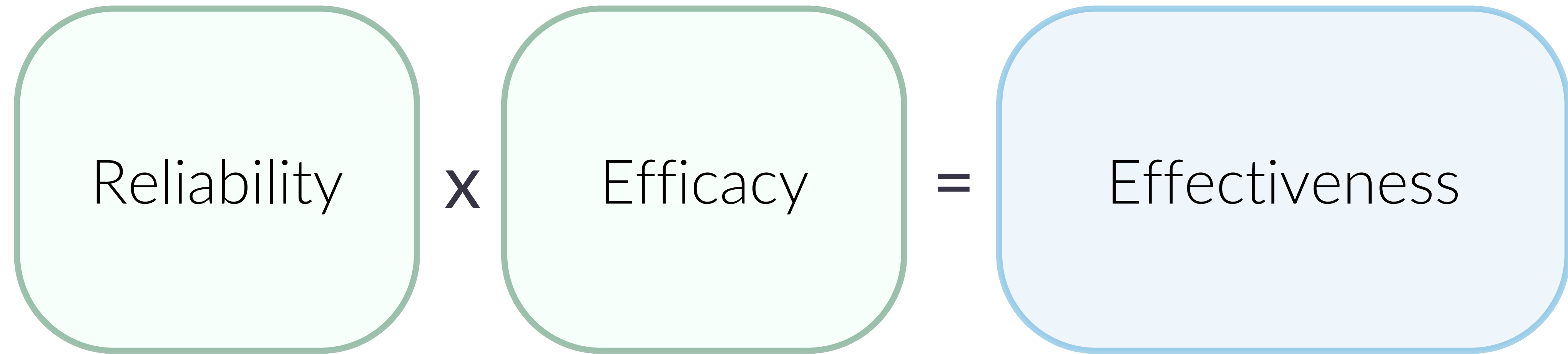
How do we gauge performance?

Reliability the probability that a sprinkler system will activate and supply water to a fire demand

Efficacy the probability that the sprinkler system will affect the development of the fire as specified in the system design objectives

Effectiveness the overall performance of the sprinkler system, combining both the reliability and efficacy

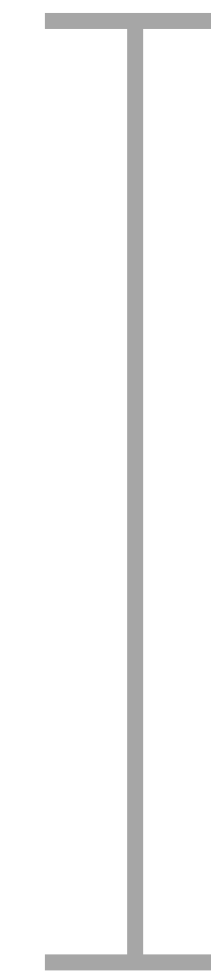
How do we gauge performance?



A review of sprinkler system effectiveness



Max



95%

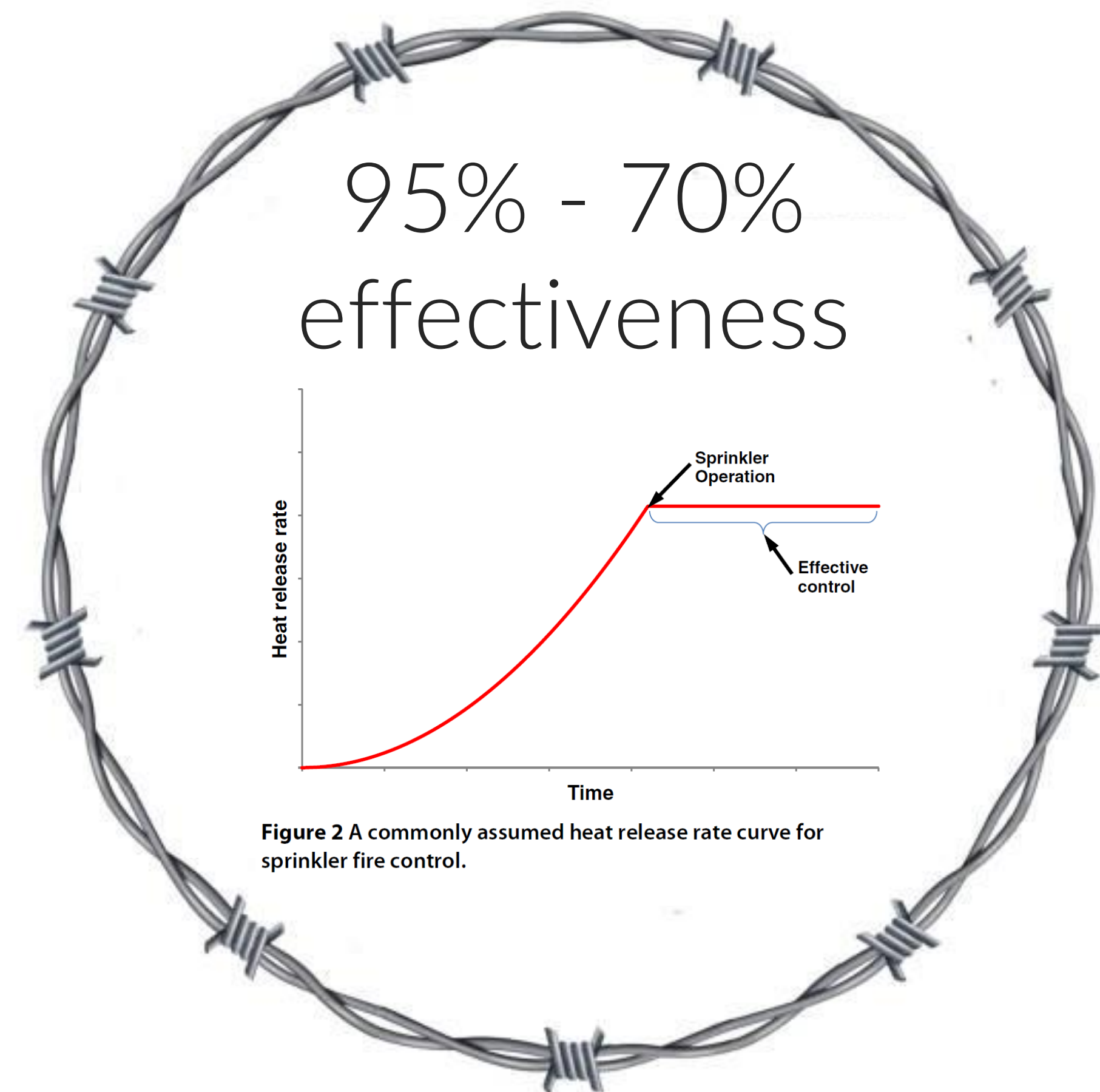
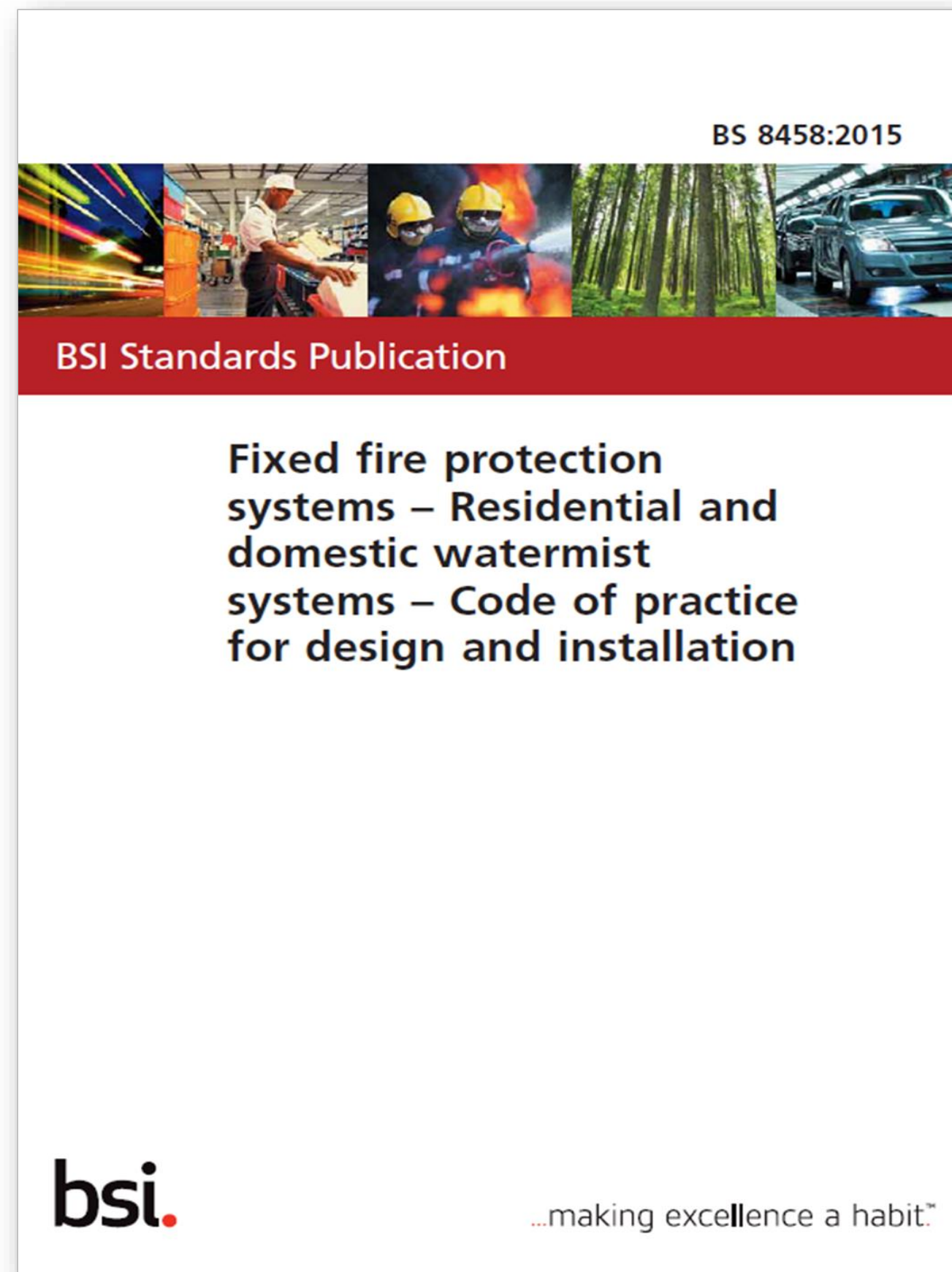
Ineffective 1 in 20

Min

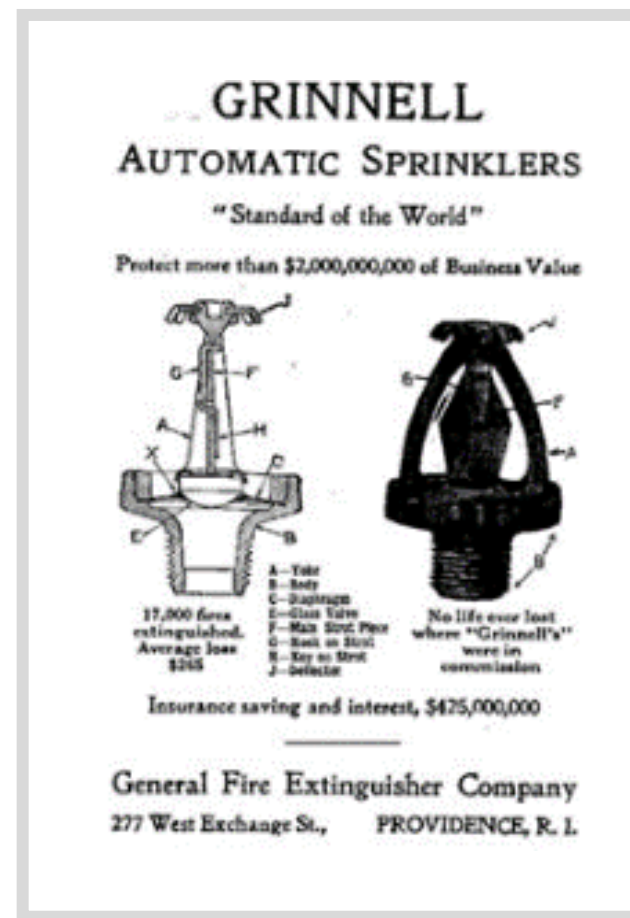
70%

Ineffective 3 in 10

Performance Benchmark



Why do we need innovation?



1882

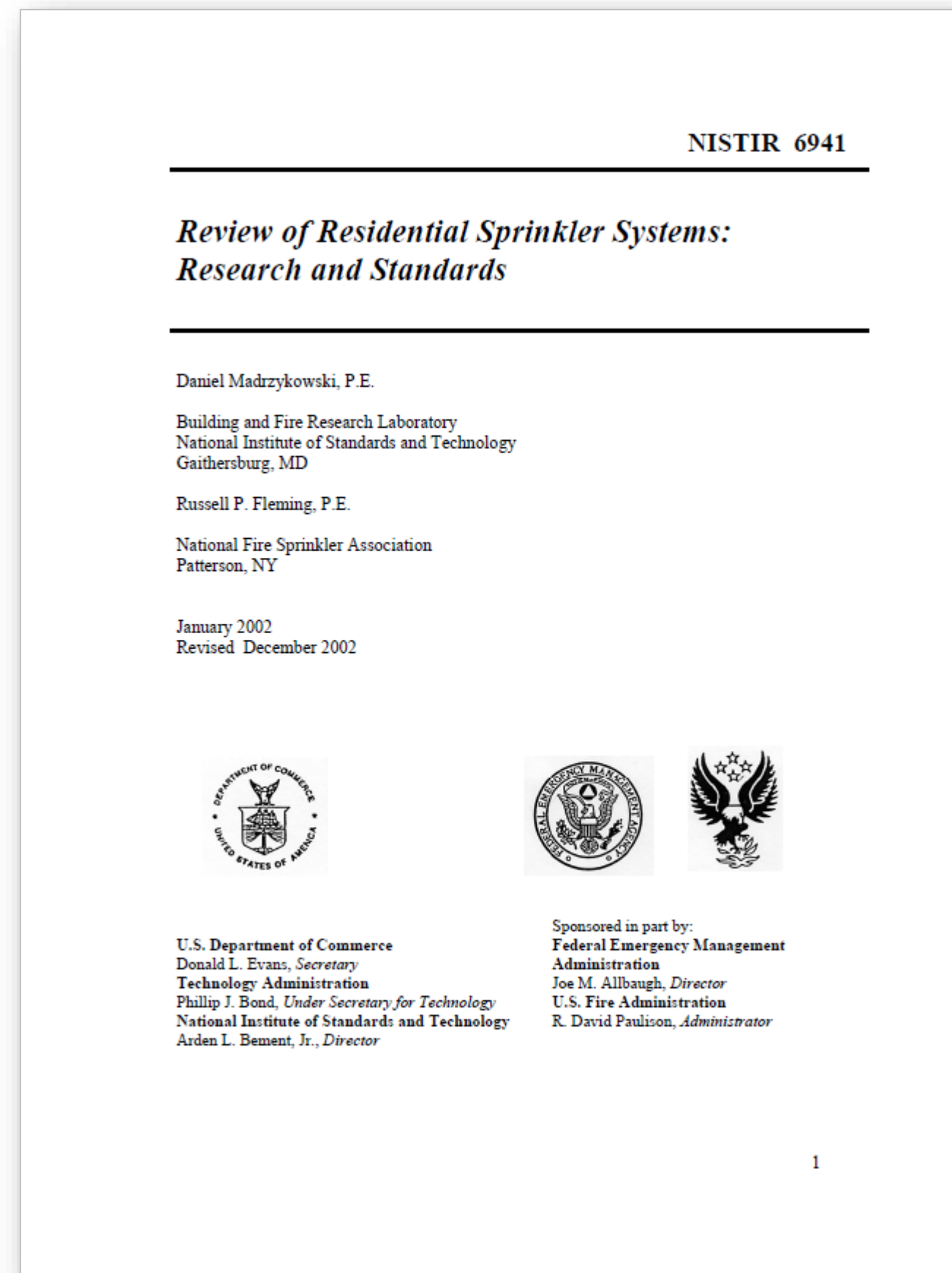
Today

A review of sprinkler system effectiveness



‘a “100% effective” sprinkler system would not equate to a 100% reduction in loss, because a fire must be present and reach sufficient size to activate the sprinkler system’

An appraisal of the ODPM



‘The research showed that a more sensitive sprinkler was needed to respond faster to both smouldering and fast-developing residential fires’

An appraisal of the ODPM

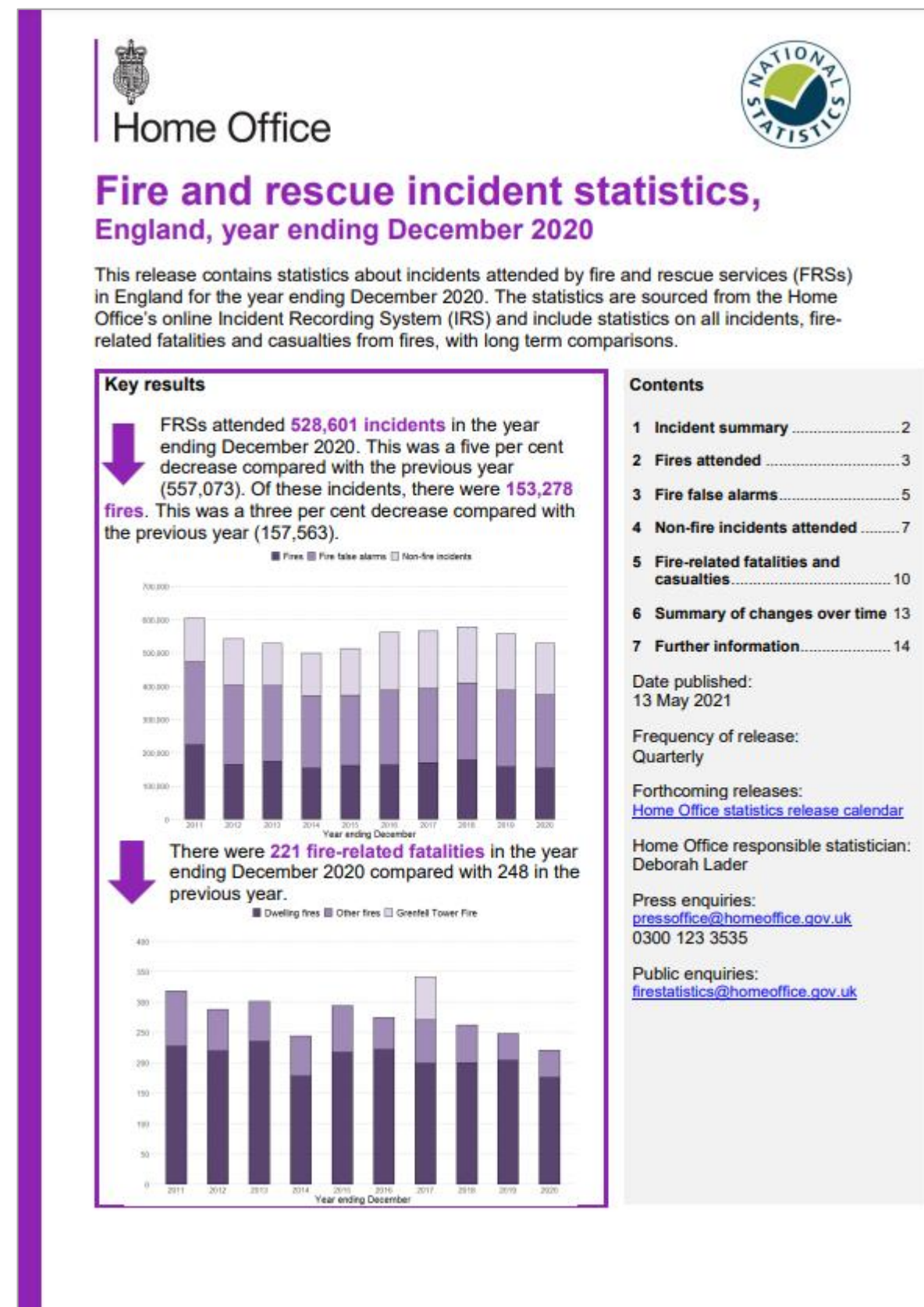


An appraisal
of the
ODPM - BRE Report

*"Effectiveness of sprinklers in
residential premises"*

'The house fires used in these tests were all of a slow-growing type that produced a lot of smoke but limited heat'

Examining fire service data



156 injuries and 5 deaths that occurred in sprinklered buildings between 2013 and 2018

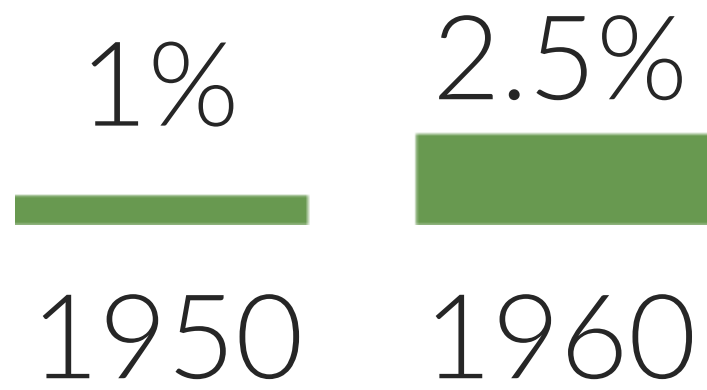
All of which were outside the life saving design parameters of the technology



Automotive Efficacy

Electronic cost as % of total car cost

“80% of innovation is electronic”



Electronic Fuel Injection

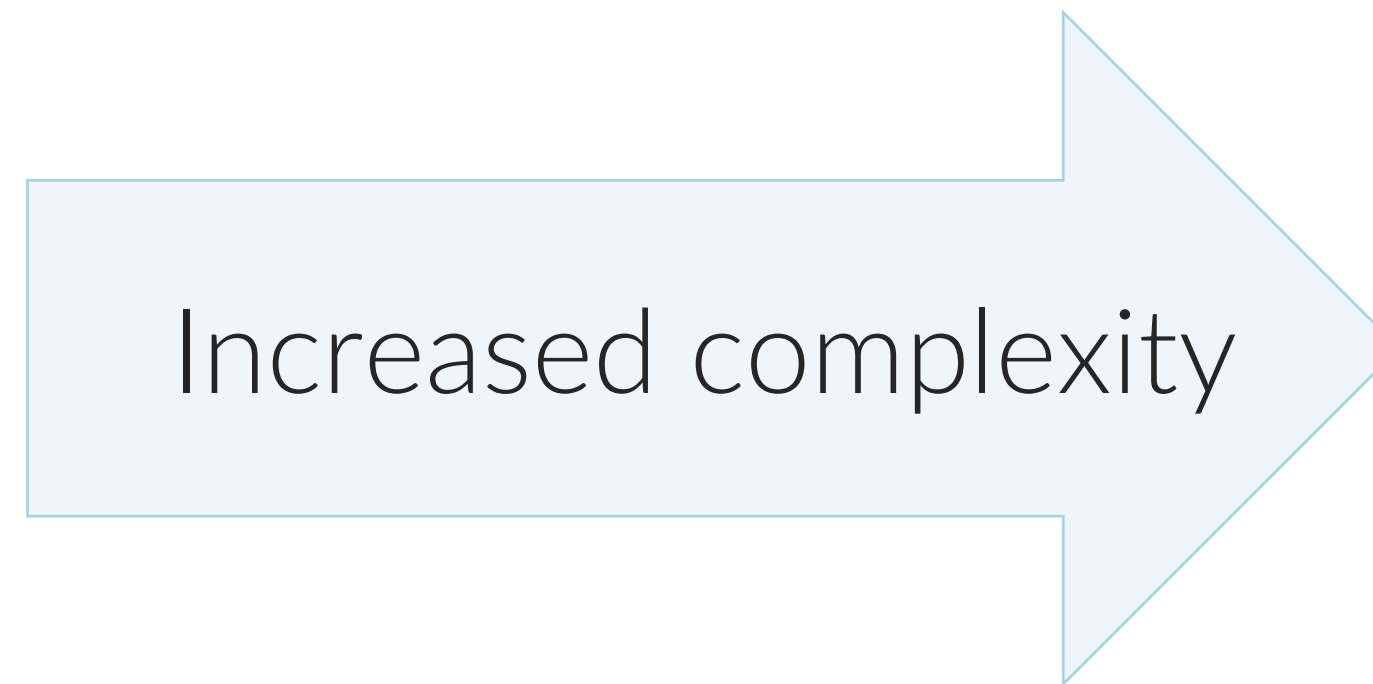
- Active- Passive Safety
- Green Powertrain
- Radar / Vision
- Infotainment
- Airbag
- ABS / ESP
- Body Electronics
- Multiplexing

1950 1960 1970 1980 1990 2000 2005 2010 2030

Automotive Reliability

- Oil change every 1,500 miles
- Solely mechanical components
- Visual inspection
- Repair of failures

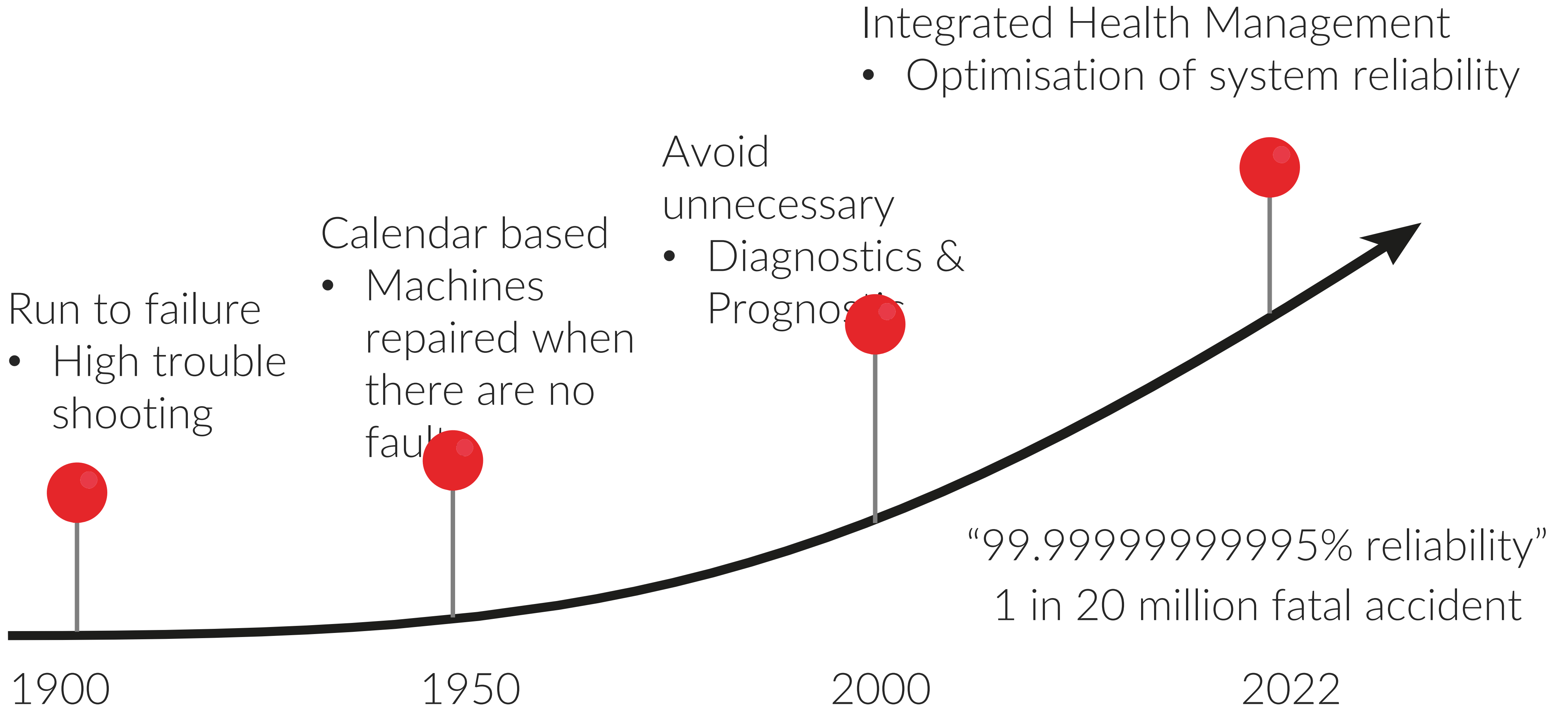
- Service interval of 15,000+ miles
- Networked electronic and mechatronic systems
- Diagnostics
- Exchange of components



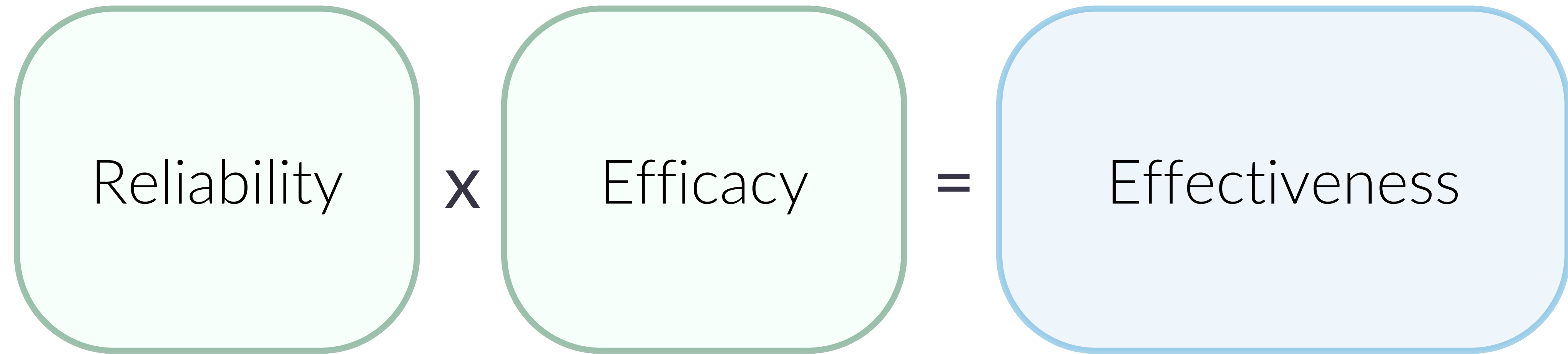
1950 1960 1970 1980 1990 2000 2005 2010 2022

Aerospace Maintenance

Increasing data volume & complexity



First principal thinking



Objective of Active Fire Suppression

Adequate level of safety for the occupants

Some limitation of the physical damage to the building

Some facilitation of firefighting



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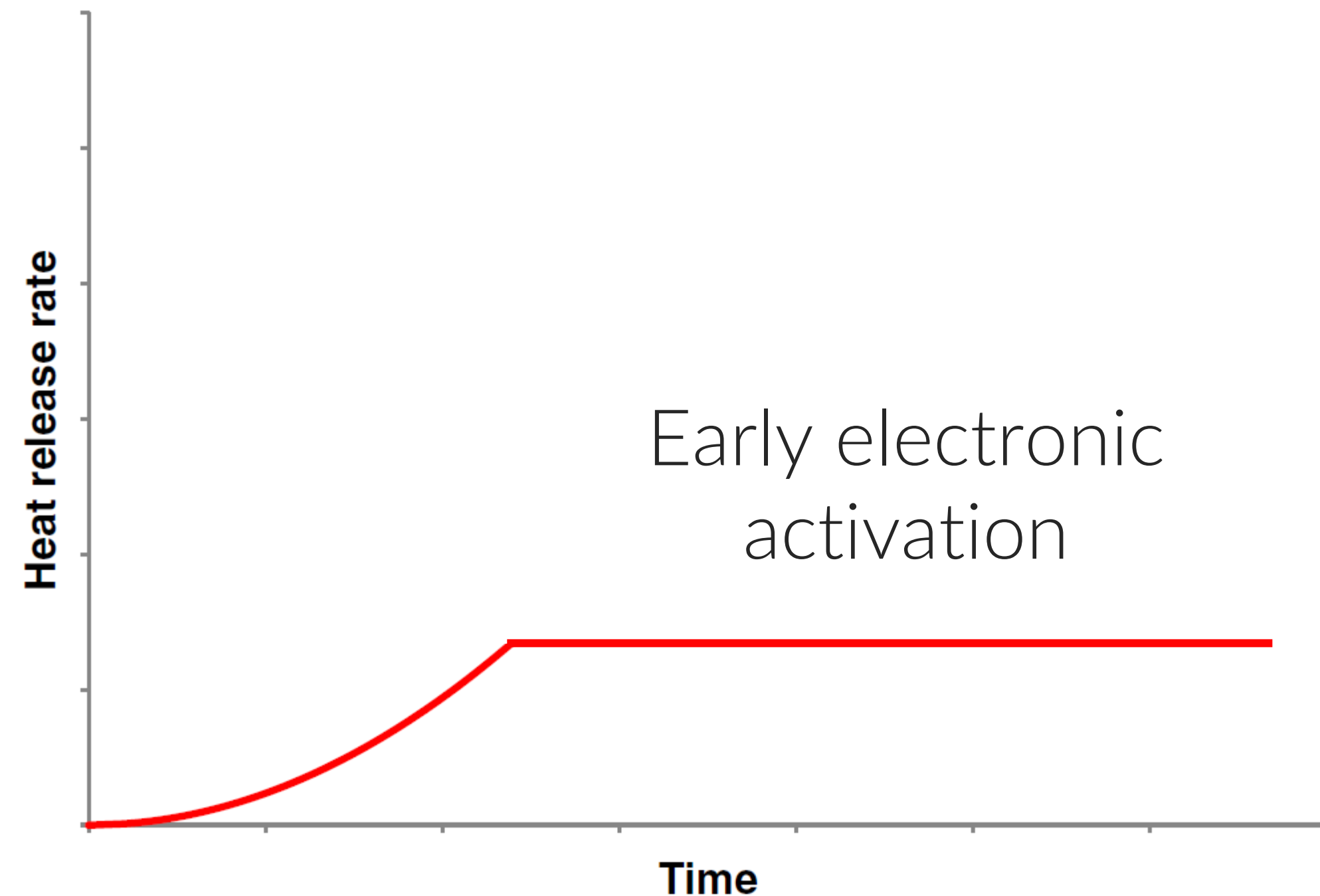
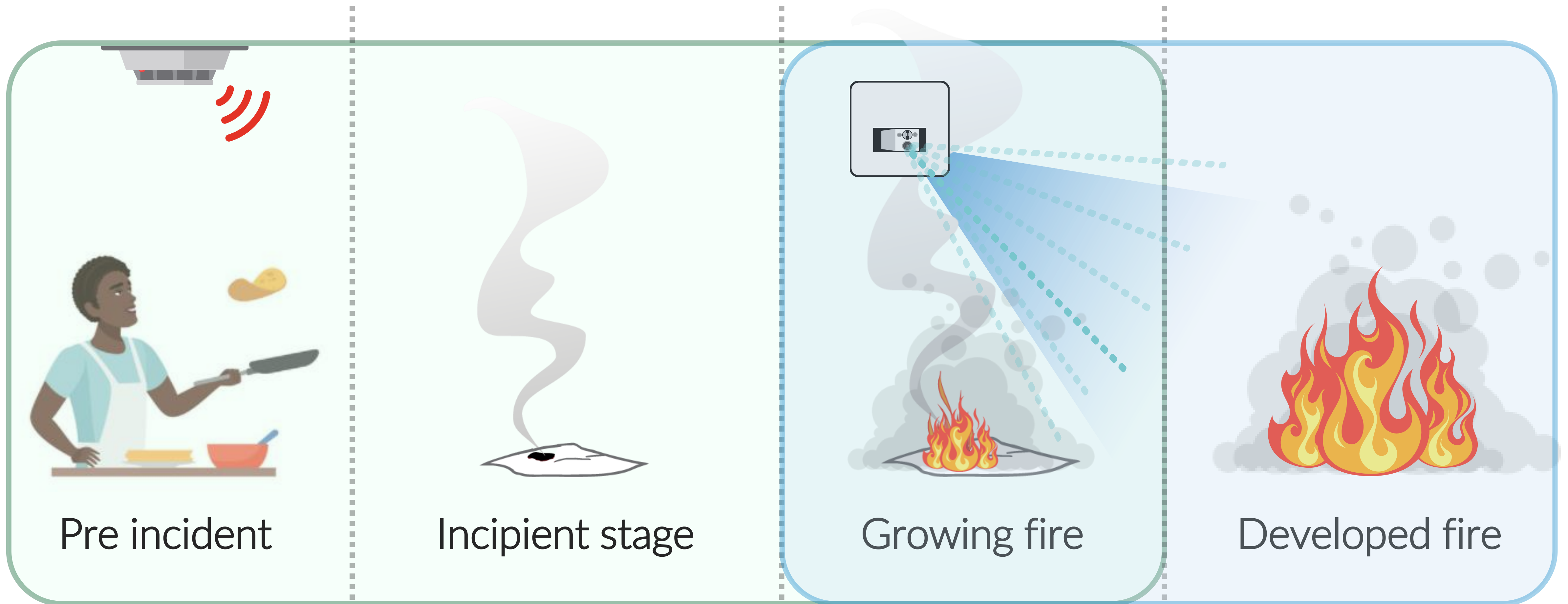


Figure 2 A commonly assumed heat release rate curve for sprinkler fire control.



Automist Smartscan
Electronically controlled
targeted watermist

Electronic activation



Automist Smartscan Hydra



Sidewall Sprinkler





Replicating the activation time of electronically controlled watermist system nozzles in B-RISK

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^b Asham Fire, Manchester, UK

^c Plumis Ltd, London, UK

ABSTRACT

This paper presents two series of enclosure fire experiments in which the activation time of electronically controlled watermist system nozzles and concealed sprinklers have been obtained. The first series experiments were aligned to the procedure given in the BS 8458 standard whereas the second series were configured to give slower growing fires than in the standard test.

The activation of the two systems have been simulated in the B-RISK zone fire model. Activation characteristics for the concealed sprinklers have been taken from elsewhere in the literature. Representative activation characteristics for the electronically controlled watermist system nozzles have been determined. The selection of these characteristics has required a balance between the results from the two experimental series. By using an effective response time index of $20 \text{ m}^{\frac{1}{2}} \text{ s}^{\frac{1}{2}}$ and an effective conductivity factor of $0.25 \text{ m}^{\frac{1}{2}} \text{ s}^{-\frac{1}{2}}$ the predicted activation times are on average 14% slower across all of the enclosure fires.

1. Introduction

1.1. Background

A report on a recent a study on the causes of fire fatalities and serious fire injuries in Scotland and potential solutions to reduce them [1] suggested that “More needs to be done in terms of reliable early detection and suitable intervention, to either delay the development of the fire or to notify people – using technology – so they can take suitable action at the early stages of the fire.” Automatic water fire suppression systems (AWFSS), such as sprinklers and watermist, provide a means to protect lives and property by both detecting a fire and then controlling or extinguishing it.

Shielded fire scenarios present a challenge to suppression systems when compared to cases in which the fire is open to the suppression medium. In the report by BRE [2] it was noted that “Sprinkler protection was not found to be a complete panacea, slow-growing and shielded fires can be a problem.” Similarly, previous work by Grosshandler et al. [3] on using water mist to protect computer cabinets found that suppressing these fires in obstructed locations is challenging.

This paper reports on two series of enclosure experiments in which the activation of a watermist system with electronically controlled nozzles has been measured. Series A consisted of BS 8458 [4] fire test configurations and Series B were ad-hoc enclosure experiments in which the fire source was configured to give a longer development time in

comparison with those in Series A, as well as considering the impact of shielding the fire. In addition to the watermist system, the Series B experiments also included measuring the activation time of concealed residential sprinkler heads.

In this paper the measured activation times of the watermist system and the concealed sprinklers have been compared. The B-RISK zone model [5] has then been used to reproduce the experiments as closely as possible, comparing simulation outputs to data for system activation time. As part of this, representative thermal sensitivity properties for the watermist system have been identified through a parametric analysis, assuming that the system can be represented as an equivalent sprinkler head. For the concealed sprinkler heads, the activation properties have been taken from the previous work of Hopkin and Spearpoint [6], with the aim to verify whether their recommended design parameters for concealed heads align with the experiments.

1.2. Electronically controlled nozzles

The concept of using an electronic means of activating a AWFSS rather than using the traditional thermally responsive elements has been discussed in the literature. Magnone et al. [7] consider the challenges posed by modern warehouse storage requirements and how ceiling-only mounted sprinklers that are electronically activated by detection and control system can provide a viable suppression solution. Kopylov et al.

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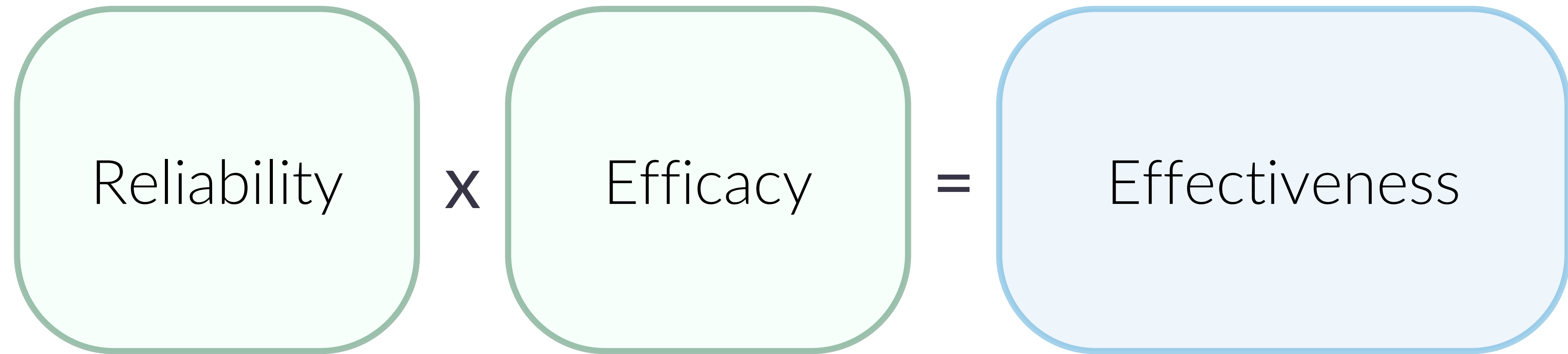
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Peer-reviewed fire engineering research

The measured activation times of a concealed sprinkler head is 2.0 to 13.7 times slower than those using an electronic nozzle system

Performance based design

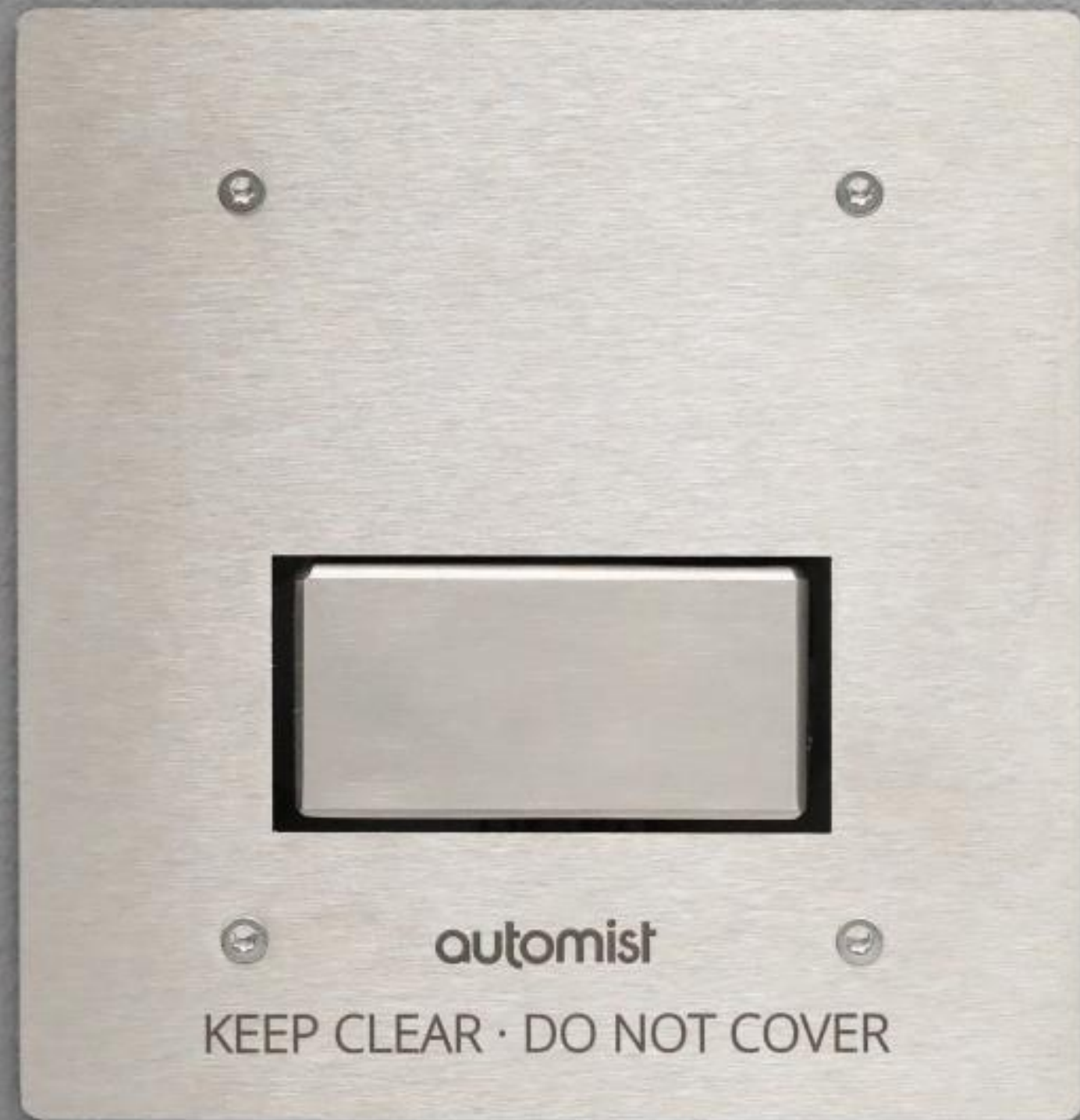


40%[?]

2-14 x faster
than a
concealed fire
sprinkler







Thank you for listening

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