

PERFORMANCE BASED ANALYSIS OF WATERMIST PROTECTION SYSTEM IN A CONVEYOR BELT USING CFD

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OUTLINE



- 1. INTRODUCTION
- 2. METHODOLOGY
- 3. PERFORMANCE CRITERIA
- 4. FIRE SCENARIOS
- 5. TRIAL DESIGNS
- 6. RESULTS
- 7. CONCLUSIONS

1. INTRODUCTION



- Conveyor belts system crucial for copper concentrate transport in mining.
- Requirement of an automatic fire protection.

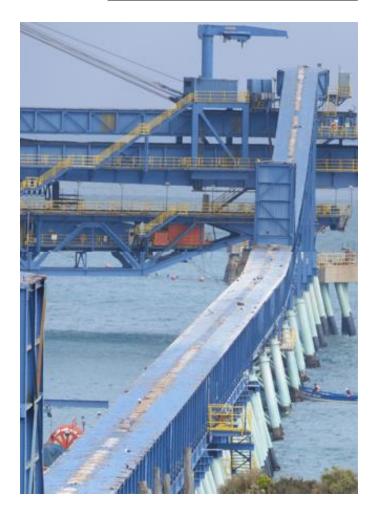




1. INTRODUCTION



• Fire protection goals of; life safety, operational continuity and minimize the **environmental impact** of water protection system discharged.





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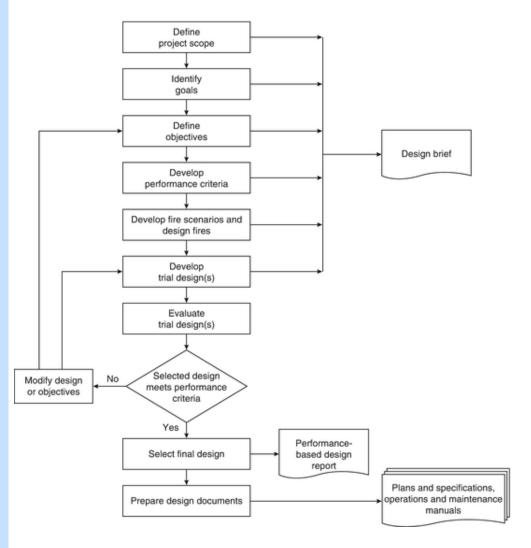
<u>Contain the water</u> discharge from the fire protection system.

<u>A bigger water flow</u> needed for fire control and extinguishment would need <u>a bigger drainage and accumulation system</u> installed in the structure of the conveyors belt above the sea.

Therefore, <u>performance base analysis</u> is developed to <u>minimize the water</u> drainage system and the potential contamination of the sea water.

2. METHODOLOGY



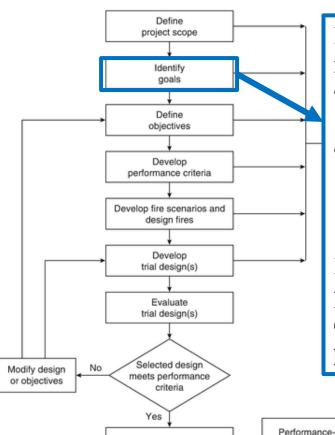


2. METHODOLOGY



General methodology for PBD according SFPE Handbook

based design report



Select final design

Prepare design documents

Provide an environment for occupants that is reasonably safe from fire by:

- **Protecting the occupants** not closely related to the initial development of the fire
- Improve the survival capacity of the occupants closely related to the initial development of the fire.

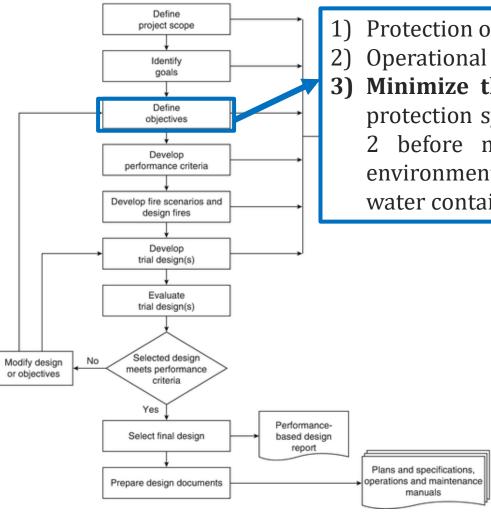
Provide an environment for the protection of property and operational continuity in the event of a fire, considering the environmental protection requirements.

Plans and specifications, operations and maintenance

manuals

2. METHODOLOGY

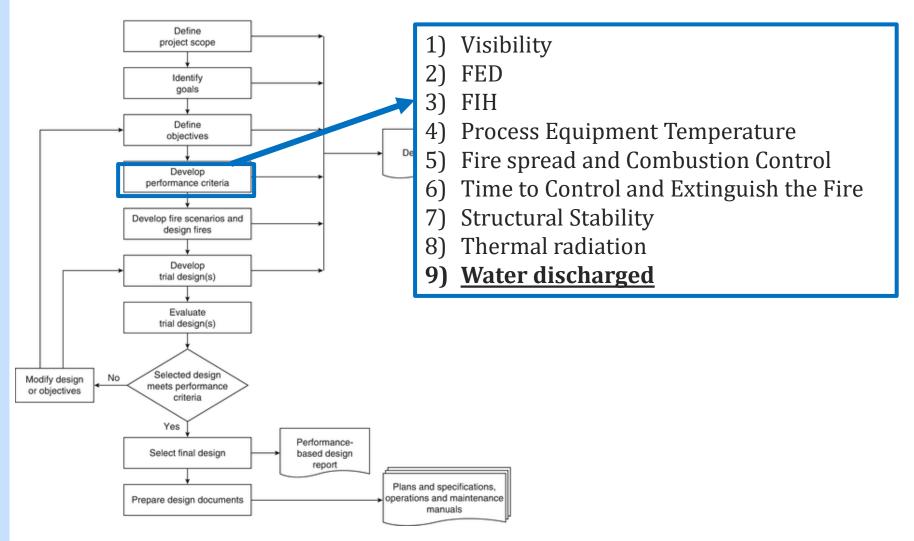




- Protection of the occupants.
- Operational continuity.
- Minimize the water discharge: evaluate a fire protection system that fulfils the objectives 1 and before mentioned and that also fulfil environmental requirements of minimize water containment.

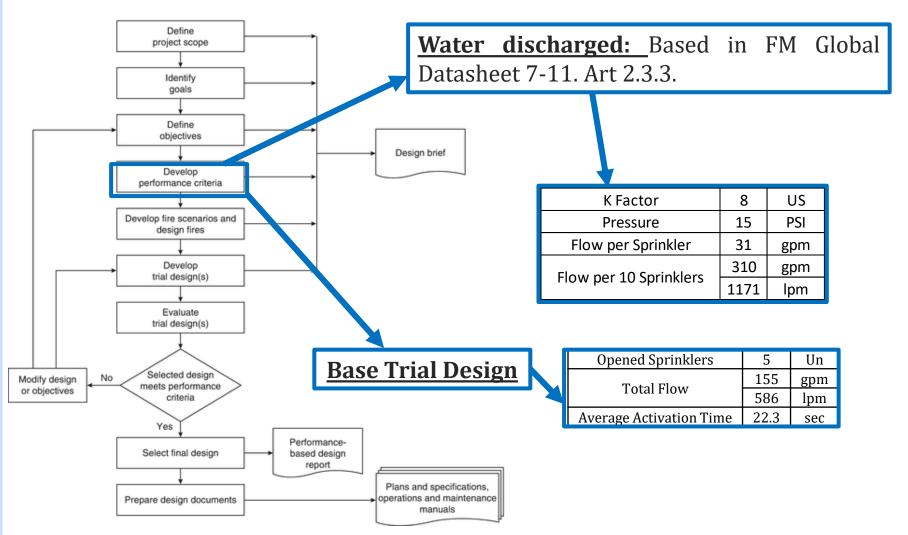
3. PERFORMANCE CRITERIA





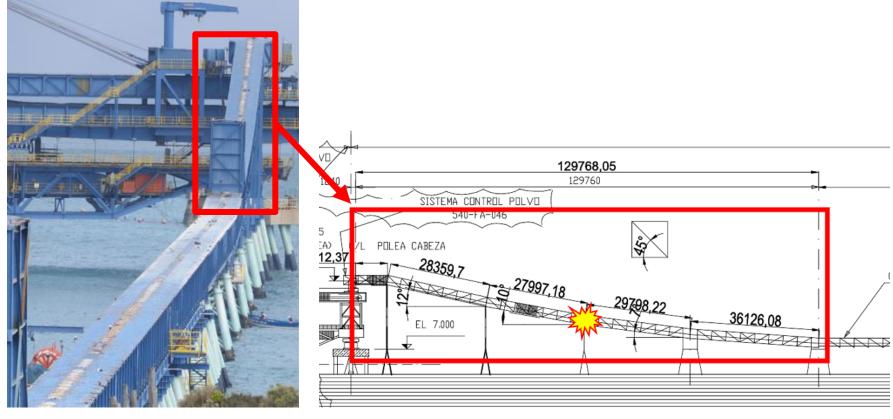
3. PERFORMANCE CRITERIA





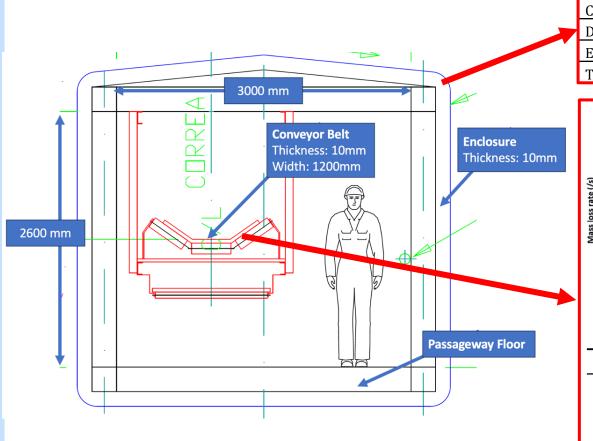


- Average 10° of slope
- 130m section
- 2 Scenarios;
- ES-01 -> Fire in the actual conditions of the facilities
- ES-02 -> Fire considering the trial designs

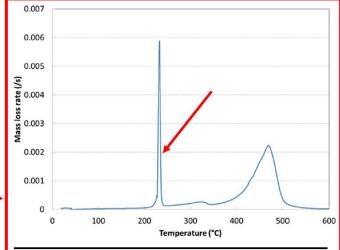




Geometry and Materials



Specific Heat	0.46	kJ/(kg°K)
Conductivity	45.8	W/(m°K)
Density	7850	kg/m3
Emissivity	0.95	Dimensionless
Thickness	0.01	Meters



Property	Virgin material
Density (kg/m³)	1300
Specific heat (kJ/kg/K)	1.3
Conductivity (W/m/K)	0.19
Heat of combustion (kJ/kg)	2.85×10^{4}
Heat of gasification (kJ/kg)	1500



Statistical Data

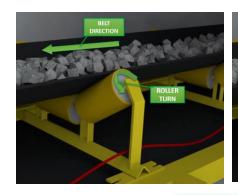
Most fires were caused by friction in the belt drive along the length of the belt, where the most common causes of conveyor belt fires were:

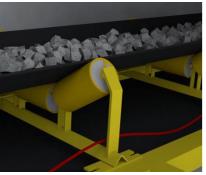
- Faulty bearing causes the excess of grease to ignite.
- Defective roller or roller causing friction and igniting the roller.
- Friction between the conveyor and a roller or pulley.
- Metal in contact with the belt.
- Rocks stuck against a roller/conveyor causing friction.

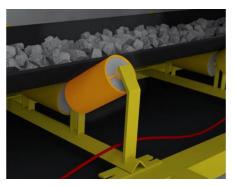
The <u>most common places</u> for fire starting are the <u>conveyor belt</u>, belt roller, return roller, impact roller, idler pulley, bending pulley and head pulley.

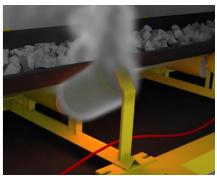


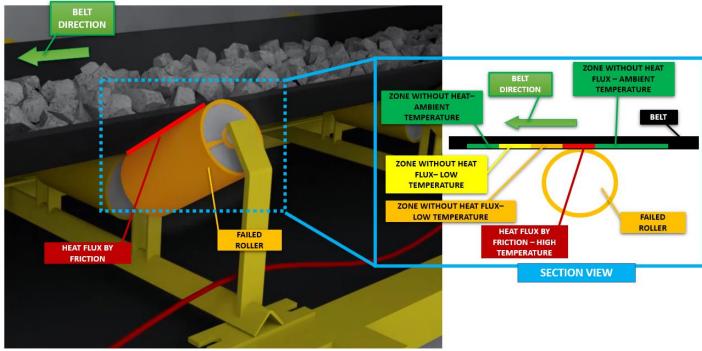
• Ignition Mode





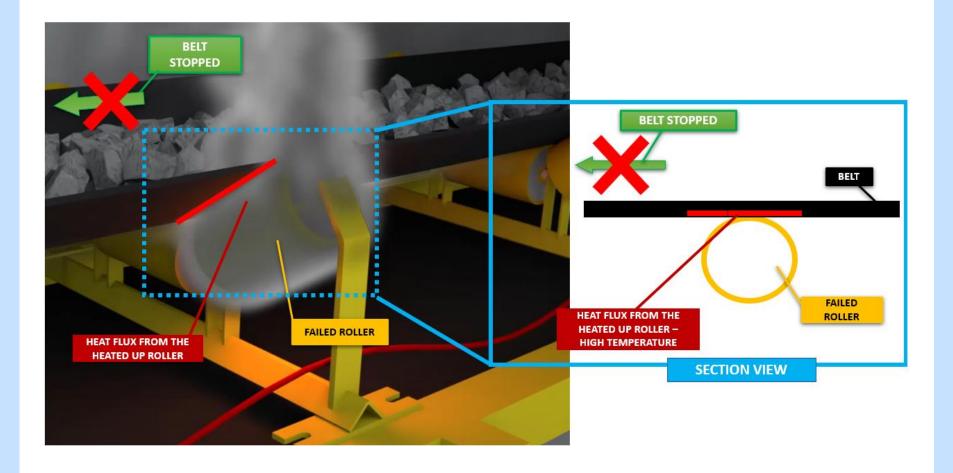






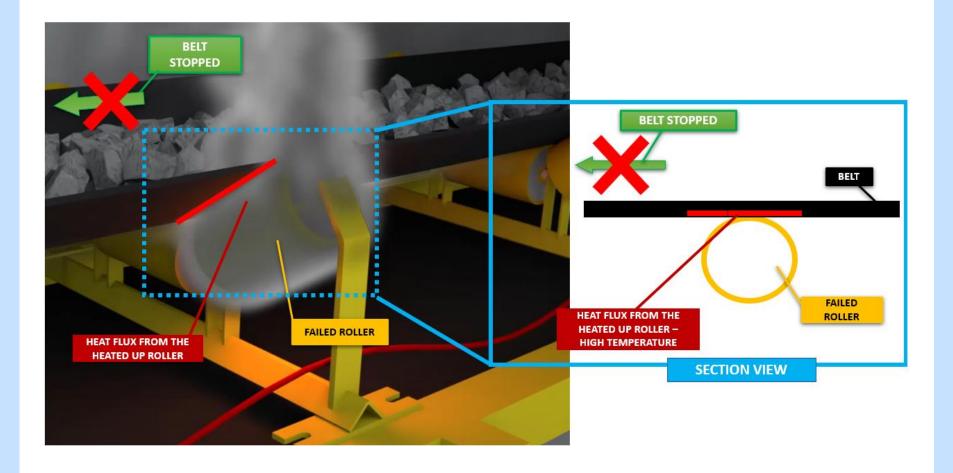


 The fire scenario considers that the conveyor belt will ignite when stops, developing a fire under no influence of the air velocity of the moving of the conveyor belt.





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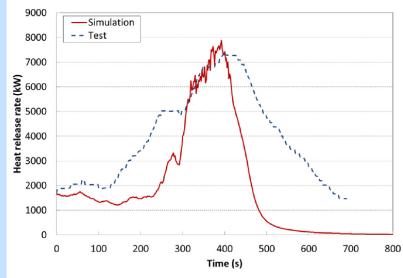


Mesh and Cell size

$$\dot{Q} = \chi \, \dot{m}^{"} A_f \Delta H_c = \chi \, \dot{m} \, \Delta H_c = \dot{m} \, \Delta H_{c,eff}$$

$$\frac{D^*}{\delta x} \to D^* = \left(\frac{\dot{Q}}{\rho_{\infty} C_p T_{\infty} \sqrt{g}}\right)^{\frac{2}{5}}$$

$$4 < \frac{D^*}{\delta x} < 16$$

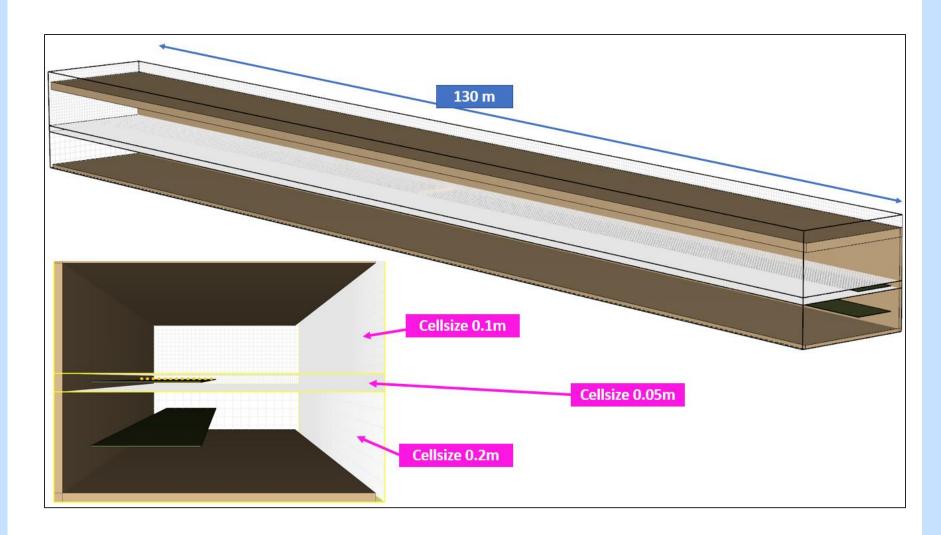


Scenario	HRR		D*	Cellsize (m)	D*/Cellsize
Scenario 01	2000	kW	0.8041	0.05	16
Scenario 02-05-A	2000	kW	0.8041	0.05	16
Scenario 02-05-B	2000	kW	0.8041	0.05	16
Scenario 02-05-C	2000	kW	0.8041	0.05	16
Scenario 02-05-D	2000	kW	0.8041	0.05	16

	Scenario	HRR		D*	Cellsize (m)	D*/Cellsize
	Scenario 01	2000	kW	0.8041	0.1	8
	Scenario 02-05-A	2000	kW	0.8041	0.1	8
	Scenario 02-05-B	2000	kW	0.8041	0.1	8
	Scenario 02-05-C	2000	kW	0.8041	0.1	8
[Scenario 02-05-D	2000	kW	0.8041	0.1	8



Mesh and Cell size



5. TRIAL DESIGNS

ES-02-05-A

- Belt with Viking sprinklers quick response
- K=8.0 (115)
- Operating pressure = 15 PSI
- Temperature rating of 165°F (74°C)
- Dv50=2274.8 um
- N° of Droplets=5000

ES-02-05-B

- Belt with Viking sprinklers quick response
- K=5.6 (80.6)
- Operating pressure = 15 PSI
- Temperature rating of 165°F (74°C)
- Dv50=1623.12 um
- N° of Droplets=5000

ES-02-05-C

- Belt with Viking sprinklers standard response
- K=5.6 (80.6)
- Operating pressure = 15 PSI
- Temperature rating of 165°F (74°C)
- Dv50=1623.12 um
- N° of Droplets=5000









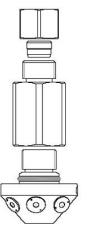
5. TRIAL DESIGNS

WMAInternational Water Mist Association

ES-02-05-C

- Open water mist system (RG Systems)
- K=2.04 lpm/bar1/2
- Operating pressure = 100 Bar
- Dv50 = 120 um
- N° Droplets = 100.000

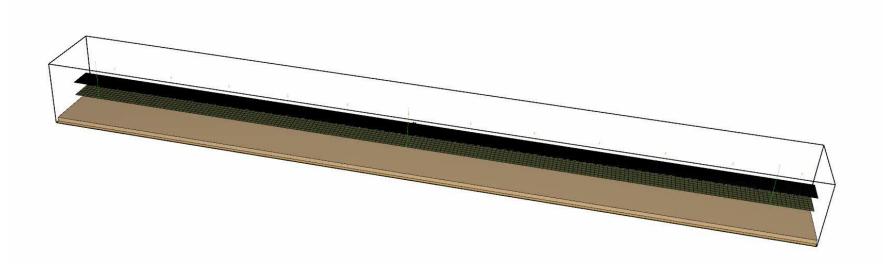




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1 Tuerca M12 / New M12 2 Anilo progresive / Progresive rise 3 Adaptate / M2 / New M13 2 Anilo progresive / Progresive rise 3 Adaptate / M2 / M	Esquema Scheme Scheme							
Characteristics technical Medio operativo / Operating medium Agua nebultzada alta presión / High pressure water mist Material del iditusor / Notros sent Material del micros / Notros sent Material del	6-	1 Tuerca M12 / Nat M12						
Material del iditusor/ Notros metals Acces Not/ Not/ Seal Material del informations of Notros Seal Material del micros Notros Seal Unión a tubería / Pipe union Mediante anilo progresivo en bicono. Tubería / Pipe union Mediante anilo progresivo en bicono. Tubería de 12x1 fisma Máxima presión de 12x3 púrsos Max. working pressure /With progresivo en bicono. Tubería de 12x1 fisma Máxima presión de 12x3 púrsos /With progresivo en bicono. Tubería de 12x1 fisma Máxima presión de 12x3 púrsos /With progresivo en bicono. Tubería de 12x1 fisma Máxima presión de 12x3 púrsos /With progresivo en bicono. Tubería de 12x1 fisma Máxima presión de 12x3 púrsos /With progresivo en bicono. Tubería de 12x1 fisma /With progresivo en bicono. Tubería de 12x1 fisma /With progresivo en bicono. Tubería /Wi	Características	técnicas			6	Microdifusor / 1	dicronozzie	
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6. RESULTS **ES-02-05-A**

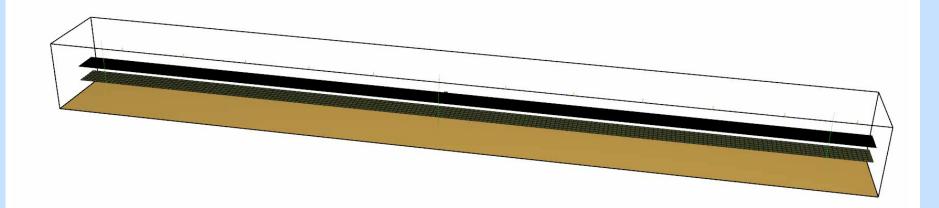






6. RESULTS **ES-02-05-B**

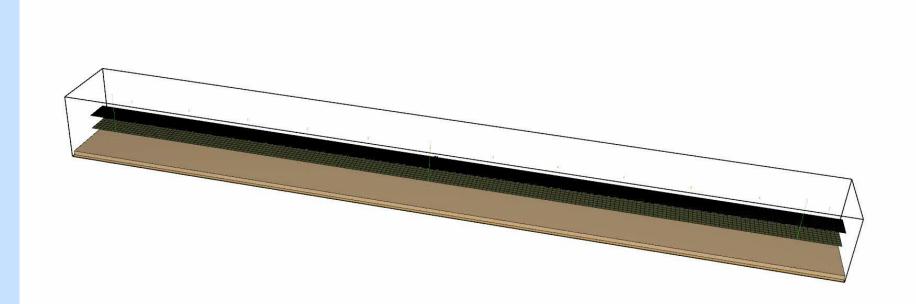






6. RESULTS **ES-02-05-C**

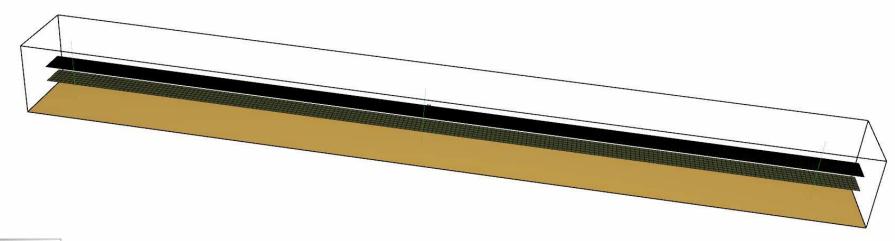






6. RESULTS **ES-02-05-D**





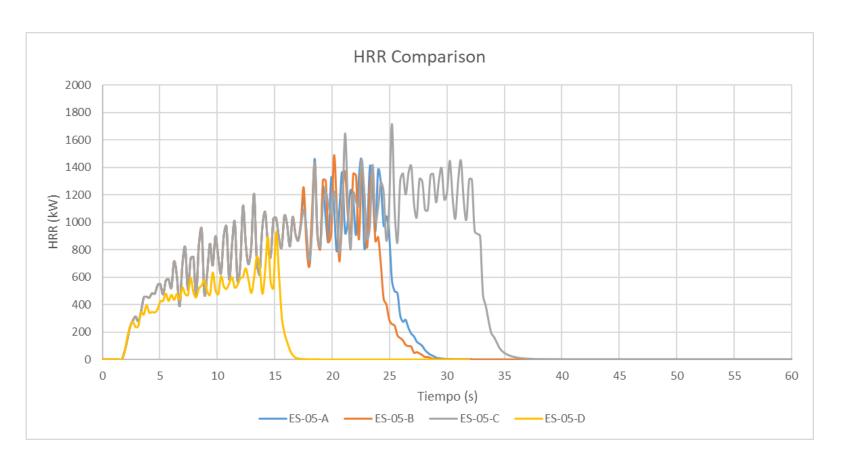


6. RESULTS



Comparison

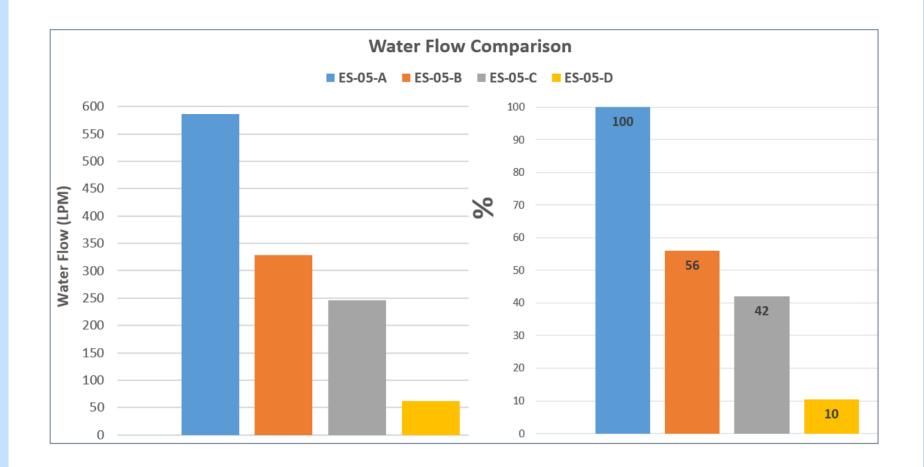
	Trial Design						
	ES-05-A	ES-05-B	ES-05-C	ES-05-D			
Average kW	584.67	565.77	607.03	338.18			
	96.32%	93.20%	100%	55.71%			



6. RESULTS



Comparison



7. CONCLUSIONS



- Sprinklers systems can control and extinguish the fire.
- Sprinkler permit to increase the HRR but use less water than the FM Global design expects.
- Water mist system can control and extinguish the fire.
- The water mist system use just 10% of the water that FM-Global expects that controls and extinguish a fire.
- Watermist Decrease size of a drainage system.
- Watermist Smaller water collector tank.
- Sprinklers HRR present average values.
- Watermist lower HRR values.
- Watermist HRR dependent on the activation time of the detection system



Thank you! Questions?

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